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GUIDANCE AND CONTROL OF TACTICAL MISSILES

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Monterey, California

THESIS

GUIDANCE AND CONTROL OF TACTICAL MISSILES

by

Thomas Alan Grote

December 1979

Thesis Advisor: D. J. Collins

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Guidance and Control of Tactical Missiles

by

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Submitted in partial fulfillment of the
requirements for the degree of

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This thesis discusses the conversion of the MOD6DF computer program for use on the IBM-360 computer at the Naval Postgraduate School. The functioning program was modified to investigate the impact miss distance for the Supersonic Tactical Missile. When the initial y-displacement error exceeded 1800 feet, the missile did not acquire the target. All errors smaller than this resulted in miss distances within 0.5 feet of the target. The midcourse guidance reference altitude was changed to reflect a sea-skimming missile. This simulation ran and impact was recorded. An attempt at adding random noise to the homing seeker was tried, but revealed that more information is required on this topic. The MOD6DF computer program was successfully converted and altered to run using the simplified ramjet model.

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TABLE OF SYMBOLS AND ABBREVIATIONS

The following is a list of the abbreviations and some of the more common fortran symbols used in the MOD6DF computer program. Each symbol is defined in two ways. The primary source of identification is by its COMMON(3415) location and the second is by its fortran symbol. The fortran symbol is not always a good identifier since it will change from subroutine to subroutine (i.e. W and WE both are used for missile weight).

A. ABBREVIATIONS

Symbol	Definition
TP	tangent plane axes
BA	body axes
SA	stability axes

B. FORTRAN SYMBOLS

Symbol	Definition
TXBA(073)	missile thrust in the x-direction in BA (lb)
TYBA(074)	missile thrust in the y-direction in BA (lb)
TZBA(075)	missile thrust in the z-direction in BA (lb)
W(086)	missile weight (lb)
S(110)	missile reference area (ft^2)
CA(111)	drag coefficient
CY(113)	side-force coefficient
CZ(115)	normal force coefficient
CBAR(116)	mean aerodynamic chord (ft)
CMQ(118)	damping in pitch coefficient
CNR(119)	damping in yaw coefficient

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Symbol	Definition
CLP(120)	damping in roll coefficient
CM(121)	pitching moment coefficient
CN(122)	yawing moment coefficient
CL(123)	rolling moment coefficient
CGI(136)	center of gravity (ft)
A(201)	moment-of-inertia about missile roll axis (x-body axis) (slug-ft^2)
B(202)	moment-of-inertia about missile pitch axis (y-body axis) (slug-ft^2)
CC(203)	moment-of-inertia about missile yaw axis (z-body axis) (slug-ft^2)
TSA(208)	angle between SA and BA (rad)
P(212)	missile angular velocity about x-BA (rad/s)
Q(216)	missile angular velocity about y-BA (rad/s)
R(220)	missile angular velocity about z-BA (rad/s)
AG(282)	unit conversion lb-slug
VXTP(286)	missile velocity in x-TP (ft/s)
XTP(290)	missile displacement in x-TP (ft)
VYTP(294)	missile velocity in y-TP (ft/s)
YTP(298)	missile displacement in y-TP (ft)
VZTP(302)	missile velocity in z-TP (ft/s)
ZTP(306)	missile displacement in z-TP (ft)
GZRO(404)	constant set to zero for flat earth gravitational field and set to one for a spherical gravitational field
ER(405)	angular velocity of earth (rad/s)
ALPO(406)	angle between north and x-TP (rad)

Symbol	Definition
OLAMO(407)	latitude origin of tangent plane
HO(414)	distance tangent plane is from earth (ft)
GO(415)	gravitational acceleration (ft/s^2)
HREF(501)	reference altitude for midcourse guidance (ft)
RE(503)	earth's radius (ft)
H(507)	altitude normal to earth (ft)
AMACH(520)	missile Mach number
THET(521)	missile pitch angle, TP (rad)
PSI(522)	missile yaw angle, TP (rad)
PHI(523)	missile roll angle, TP (rad)
GAMMAV(527)	vertical flight path angle, TP (rad)
VEL(528)	magnitude of missile velocity (ft/s)
VAT(529)	missile velocity (ft/s)
TF(550)	program termination time (s)
VAH(561)	computed speed of sound (ft/s)
ALAT(576)	latitude of target position (deg)
AZ(578)	azimuth of target position (deg)
DYNP(581)	dynamic pressure (psi)
FLGRJ(606)	constant set to zero indicates run will use ENGINE subroutine and when set to one run will use RAMJET subroutine (simplified ramjet model)
T(932)	actual time (s)
T1(933)	boost engine ignition (s)
T2(934)	commence acceleration command mode (s)
T3(935)	boost engine burn-out/port cover blow-in (s)
T4(936)	start ramjet engine (cruise) (s)
T5(937)	commence heading and altitude guidance control (s)

Symbol	Definition
T6(938)	commence terminal dive (s)
T7(939)	commence terminal guidance - search (s)
T8(940)	commence terminal guidance - track (s)
DMAX(1740)	maximum fin deflection (rad)
CPP(2669)	time between printouts (s)
ROLLO(2901)	initial roll angle (rad)
PITCHO(2902)	initial pitch angle (rad)
YAWO(2903)	initial yaw angle (rad)
STEP(2905)	determines executive program flow after staging
DOC(2909)	defines number of times COMMON will be printed
HMIN(2911)	minimum integration step size
HMAX(2912)	maximum integration step size
DER(1)(2913)	integration step size (s)

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I. INTRODUCTION

Research was undertaken to convert the MOD6DF computer program received from NWC China Lake for use on the IBM-360 computer at the Naval Postgraduate School. Once a functioning program was obtained, initial displacement error versus impact miss distance was investigated for the supersonic tactical missile. Additionally, the midcourse guidance reference altitude was changed to reflect a sea-skimming scenario and this was examined for its effect on the terminal guidance problem. This report not only discusses the aforementioned topics, but also describes the missile mission requirements and the MOD6DF computer program.

II. MISSION REQUIREMENTS

The Supersonic Tactical Missile (STM) mission is divided into six phases (Ref. 1).

* initial conditions
* separation
* boost
* transition
* cruise
* terminal

These divisions are based on the missile aerodynamics. The initial condition phase establishes the starting conditions for each launch. This is done while the missile is still attached to the launch platform. The separation phase starts when the missile is launched. The missile falls for approximately five seconds until the boost engine ignites. This initiates the boost phase which continues until the missile achieves Mach two. As the missile passes through Mach one, plume effects are encountered which the aerodynamics account for. At the end of the boost phase, the port covers blow in. This initiates the transition phase. This phase is very short and allows the debris to be ejected from inlet ports. The cruise phase commences when the ramjet engine ignites. This engine propels the missile until target impact. The terminal phase of the flight begins when the missile is commanded to dive from the cruise altitude. This phase concludes when the flight is terminated at target impact.

The six STM mission phases require four phases of control. These control phases are:

* separation

* midcourse guidance

* terminal dive

* terminal guidance

The four Guidance, Navigation, and Control (GN&C) system control phases
are directly related to the mission phases. Figure 1 displays this
relationship (Ref. 2). To obtain a successful flight, various types of
control and guidance functions are required. Figure 2 (Ref. 3) illus-
trates the guidance control mode sequencing in relation to the mission
phases and also indicates the critical missile switching times. The
control phases are discussed below, along with the appropriate guidance
modes.

A. SEPARATION

The separation phase commences upon launch. The missile is ejected
downward from the launch platform. Additionally, the pitch attitude of
the missile is commanded down. Since this portion of the flight is
unguided, the ejection force and gravity are the only forces acting on
the missile. At launch, the missile is required to be in the attitude
command mode.

Five seconds into the flight, the missile pitch attitude is commanded
up and the boost engine is ignited. The booster continues until the
missile attains Mach two, at which time control is shifted from attitude
to acceleration control mode. The acceleration control then requires
the missile to maintain the normal and lateral accelerations at zero.

The last event to occur in the separation phase is inlet port cover
blow-in. The time delay that allows the port covers to clear is a func-
tion of altitude.

CONTROL PHASES/MISSION PHASES
RELATIONSHIP

FIGURE 1

t_0 - LAUNCH: START SIMULATION

t_1 - BOOSTER IGNITION

t_2 - CONTROL SYSTEM MODE CHANGE FROM ATTITUDE TO ACCELERATION CONDITION AT M=2.0

t_3 - PORT COVER BLOW-IN, BOOSTER BURNOUT

t_4 - RAMJET IGNITION, t_3 + .3 sec

t_5 - ENGAGE FUIDANCE MODES

t_6 - DIVE COMMAND

t_7 - SEEKER SEARCH MODE IS ACTIVATED

t_8 - TERMINAL TRACKING

FLIGHT MODE SEQUENCING

FIGURE 2

B. MIDCOURSE GUIDANCE

Midcourse guidance begins upon completion of the separation phase. The moment the port covers are clear, the phases shift. During this phase two things are required. The GN&C must guide the missile to the established cruise altitude and then guide the missile (in the horizontal plane) to the predetermined target location.

To accomplish these requirements the GN&C system employs both altitude and heading control. The altitude control acts upon the pitch axis to drive the missile to the cruise altitude and then to maintain that altitude until the terminal dive phase commences.

The actual guidance work is performed by the yaw axis. The GN&C system uses the heading control to steer the missile to the target position. To generate the steering commands a guidance law is necessary. The guidance law should minimize the cross-track error and the final lateral acceleration. A minimum cross-track error allows for minimum flight time and minimum displacement error when target search is initiated. Minimizing the final lateral acceleration ensures that the seeker will continuously be pointing toward the target area. To insure accuracy, the guidance law must be able to perform these functions when subjected to disturbances such as wind and thrust misalignment.

C. TERMINAL DIVE

The terminal dive phase commences when the missile is commanded to dive. The actual time that this command is given is a function of the predetermined target coordinates. Upon diving, the missile must accelerate downward along a 60-degree (from horizontal) dive angle to the target position. Once the missile has steadied up in the proper dive aspect, terminal guidance commences.

D. TERMINAL GUIDANCE

During the terminal guidance phase the seeker is required to search, acquire, and track the target. The GN&C system then uses these tracking signals to direct the missile to the target. The seeker uses a preprogramed search pattern to locate the target. When the target has been acquired, the seeker then commences tracking it and also notifies the GN&C system that the target is being tracked.

Target acquisition takes place when the target falls within the instantaneous four-degree beamwidth pattern as it traverses the scan pattern on the earth's surface. The computer program uses this assumption since the exact missile target acquisition mechanism has not yet been defined.

Upon acquisition, the GN&C system closes the seeker tracking loop. The radiometer error signal is defined as the difference between the look vector and the line-of-sight. This signal is used to reposition the antenna gimbals so the look vector and the line-of-sight coincide. Under the closed loop operation the radiometer output is proportional to the line-of-sight rate and this is the signal used to guide the missile to target impact.

III. COMPUTER SIMULATION

The modularized six-degree-of-freedom (MOD6DF) computer program was developed by the Litton Systems, Inc., Guidance and Control Systems Division (Ref. 4) to be used in analyzing missile guidance and control. The program uses a building block approach, where each module corresponds either to a missile subsystem or an environmental system. In its original form, the program is used primarily for terminal guidance of air-to-surface missiles. The Naval Weapons Center, China Lake modified the original program to specifically apply to the Supersonic Tactical Missile (STM). The modification also allows the user the capability of simulating any portion of the missile flight trajectory.

The MOD6DF computer program consists of four main decks and one auxiliary deck. The main decks include the executive programs, operational subroutines, modules, and input data deck. All the subprograms utilized in the integration and the sequencing of the modules are contained in the executive programs. The operational subroutines are used by the user to control the program while it is running. The psysical system and the environmental subroutines are included in the modules. The input data deck contains all the information the executive programs need to execute the desired run. Lastly, the auxiliary deck consists of all those subprograms (subroutines and functions) that are required by the modules.

Once the user starts making simulations, he must concern himself with program sequencing. Proper sequencing is required to ensure a valid run is achieved. Since it is of such importance, sequencing will be discussed as the final part of this section.

A. EXECUTIVE PROGRAMS

The executive programs are the main core of the MOD6DF program. These subroutines have various functions in setting up, sequencing, integrating, and resetting the program. Since these functions are required by any type of analysis done, the user should never have to change any of these subroutines. Reference 5 should be consulted if the user desires more information about the content of any of the subroutines described herein.

1. Zero

Subroutine ZERO is used to set all the COMMON(3415) locations to the value zero. This is done to ensure that no erroneous information is used in the simulation.

2. Oinpt1

Subroutine OINPT1 is the basic input routine for the MOD6DF program. The normal input is from punched cards. However, inputs may also be read from tapes. The basic input cards will be discussed in the section covering the input data deck.

3. Auxi

Subroutine AUXI is used to call the initialization modules for each run. Additionally, it sets up the list of state variables which are used in AMRK.

4. Auxsub

Subroutine AUXSUB is used to call the dynamic modules. In calling the dynamic modules, AUXSUB sets and resets the lists needed for AMRK and the COMMON(3415) storage cells with the most recent values of the state variables and their derivatives.

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5. Amrk

Subroutine AMRK is the integration subroutine. It uses a point-wise first order Runge-Kutta method. All the state variables to be integrated must be listed in COMMON(3415) and also must appear in a processing list.

6. Reset

Subroutine RESET is used to reinitialize up to fifty input parameters. This is done prior to the start of any repeated runs. To indicate which parameters are to be reset, the number one is punched in columns 46-60 on the respective type three card.

7. Return Group

The return group is a collection of all the unused modules. Since all the modules and their initialization modules are called by AUXI and AUXSUB, the unused ones must still remain in the deck. These are required to ensure proper linking when the computer attempts to link all the subroutines. All the subroutines in this grouping contain three cards. The three cards are the subroutine title, and a return and an end card.

8. Sub11, Sub12, Sub13

These subroutines are used to call the operational subroutines that are required. They call the routines in the order prescribed by the input data deck. The number at the end of each subroutine title indicates which operational subroutines it can call. For example, SUB11 can call STGE1.

B. OPERATIONAL SUBROUTINES

The operational subroutines provide the user with control of the program while it is running. The order in which the operational subroutines are called is specified by the input data deck. Since these routines assist the user in controlling the simulation, they can be reprogrammed. However, it is advised that they not be changed until the user has become quite familiar with the overall operation and sequencing of the MOD6DF program. For more in depth knowledge of the operational subroutines the user should consult Ref. 6, and the computer listing, which is contained at the end of this report.

1. Inpt1, Inpt2, Inpt3

These subroutines are available for new inputs during the simulated flight. The only one presently used in the program is INPT1. It is utilized to input a namelist file which is used by ENGINE and is described there.

2. Oupt1, Oupt2, Oupt3

These subroutines allow for the print-out of up to fifty different variables during the flight simulation. OUPT1 is not utilized in the deck. OUPT2 is used when the desired output is to be put on tape. OUPT3 is the basic output routine. It prints the desired output on regular computer paper.

3. Stge1, Stge2, Stge3

These subroutines allow for proper staging, run termination, etc.. Presently STGE1 is not being used. STGE2 is being used as the staging initialization subroutine. STGE3 is the primary subroutine of this group. It stages when impact with the earth is made, when the final time, TF(550), is reached, or when LCONV(2672) is set equal to two. All the tolerances for staging are listed in STGE3.

4. Cntr1, Cntr2, Cntr3

These subroutines allow the external dynamic control inputs to the modules. In the MOD6DF program these are not used.

5. Rndm1, Rndm2, Rndm3

These subroutines allow random noise to be added to the state variables generated in the modules. RNDM1 is not used in the program. RNDM2 is used as the initialization subroutine, while RNDM3 provides continous noise values. These subroutines produce correlated noise values for as many modules as required. The noise values remain fixed during each individual integration cycle.

6. Auxa1, Auxa2, Auxa3
   Auxb1, Auxb2, Auxb3
   Auxc1, Auxc2, Auxc3

These subroutines are auxiliary routines that allow for external input, output, control, etc. of the modules. At the present time, none are utilized in the MOD6DF program.

C. MODULES

The modules are of prime importance to the user since they represent the 'model' of the dynamic system. In general, the model is described by ordinary non-linear time-varying differential equations with both random and deterministic forcing functions. The user must first reduce these equations to an equivalent system of first order equations, which can then be described by each module. Generally speaking, the physical system is so complex that this would be impossible to do. However, due to the modularity of the MOD6DF program, the user can think of each module as a completely independent system described by the equations within that module.

There are thirty-six possible modules divided into five functional

categories. Each group is identified by a letter which pertains to that groups function; A (airframe), C (computers), D (dynamics), G (geophysical), S (sensors). A complete printing of each module is contained in the computer program listing.

1. Airframe

   a. Subroutine A1

   This is the aerodynamic forces and moments modules. It calculates all the necessary forces and moments in body axes. These values are then used in the computation of the dynamics.

   b. Subroutine A2

   This is the missile aerodynamic coefficient module. It calculates the required coefficients using the information stored in the BLOCK DATA. Using the timing inputs, this routine computes the coefficients for the different effects. Some of the effects accounted for are; plume, separation, and control surfaces effectiveness. With this done the total coefficients are determined.

   c. Subroutine A3

   This is the missile propulsion module. The timing inputs are used to determine whether the missile is in free fall, boost, transition, or cruise phase. With this determined the correct engine subroutine (BOOST, RAMJET, ENGINE) can be called. Three variables are calculated using the body axes as the frame of reference. They are the missile thrust is all coordinate directions, the principal moments of inertia, and the missile weight.

   d. Subroutine A4

   This is the fin actuator module. The four control surfaces commands are calculated as either ideal actuators or as second-order

ones. In addition to control surfaces commands, the rate of change of yaw, and roll are computed.

e. Subroutine A5

This module is part of the return group.

2. Computers

a. Subroutine C1

This is the autopilot module for the STV-G. It uses the cruise engine ignition time to divide the routine into boost/separation and cruise phases. These two phases use different algorithms to calculate the turning moments in pitch/yaw and roll.

b. Subroutine C2

This is the guidance command module. Using the timing inputs, this routine is divided into separation/boost, dive/climb, cruise, terminal dive, and terminal homing sections. Each section uses slightly different algorithms to calculate the guidance commands to maintain the proper flight profile.

c. Subroutines C3 - C10

These modules are part of the return group.

3. Dynamics

a. Subroutine D1

This is the translational dynamics module. It computes the total acceleration in body axes and then converts them to the tangent plane reference. Then, accounting for aerodynamics, thrust, gravity, and coriolis, the velocity and acceleration are calculated.

b. Subroutine D2

This is the rotational dynamics module. With the principal axes as a reference, this subroutine computes the body angular rates and the attitude direction cosines.

c. Subroutines D3 - D5

These modules are part of the return group.

4. Geophysical

a. Subroutine G1

This is the gravitational and coriolis acceleration module. It calculates the gravitational acceleration using one of two fields. The user specifies the field to be used by an input card. To use a flat-earth gravitational field, GZRO(404) must equal 0.0, and to use a spherical gravitational field, GZRO(404) must equal 1.0.

b. Subroutine G2

This module is part of the return group.

c. Subroutine G3

This is the air data module. It computes the velocity, in all three coordinate directions, with respect to the air mass. These values are then resolved into body and stability axes. This module also computes all the properties of air by calling subroutine AIR. These values are stored in their COMMON(3415) locations for use in the other modules.

d. Subroutine G4

This module is part of the return group.

e. Subroutine G5

This is the coordinate conversion module. It takes the missile position, does a coordinate conversion and then it determines the position, velocity, and acceleration in the ECI system.

f. Subroutine G6

This module is part of the return group.

5. <u>Sensors</u>

    a. Subroutine S1

This is the homing seeker module. It simulates the missile seeker and computes the seeker dynamics and Euler angle rates. Several flags are used to control the seeker sequencing:

    (1) <u>FLAGS(335)</u>. FLAGS signals the start of the seeker search.

    (2) <u>FLGT(317)</u>. FLGT signals when the seeker is locked-on.

    (3) <u>FLGTS(347)</u>. FLGTS signals the end of search.

    (4) <u>FLGD(336)</u>. FLGD signals when the seeker has detected the target.

    (5) <u>FLAGLT</u>. FLAGLT signals when the target is outside the seeker field of vision.

    b. Subroutine S2

This is the radiometer module. It takes the target position and the ATIGS target position and converts them from body axes to the seeker axes. Using target position, the module then calculates the azimuth and elevation error signals.

    c. Subroutines S3, S4

These modules are part of the return group.

    d. Subroutine S5

This is the accelerometers and gyros modules. The user has the option of using ideal or digital accelerometers. To specify the type of accelerometer, the user must include the appropiate data statement in the subroutine. If ideal accelerometers are desired, FLGA must equal 0.0 and for digital accelerometers, FLGA must equal 1.0.

    e. Subroutines S6 - S10

These modules are part of the return group.

D. INPUT DATA DECK

The input data deck provides the user with the means of specifying
which operational subroutines and modules are to be utilized for the
desired run. It also allows the user to set the starting conditions.
In general, only the constants and the state variables must be given
initial values. All quantities in COMMON not given initial values will
be set to zero by ZERO. In addition to the state variables, the upper
and lower error bounds must be initialized. There are seven types of
input cards, each indication a certain function.

Type	Function
0	read/write tape
1	operational subroutine to be called
2	module to be called
3	numerical input
4	printed output
5	parameter square and sum
6	termination and random noise generator input

A separate card is required for each subroutine, module, input, and
output quantity. A sample computer printout of the input data deck is
contained in the computer output section.

1. Type 0 Card

Type 0 cards are used to indicate if the type 3 inputs are to be
read from or written onto an auxiliary tape. These procedures can be
used rather than reading the inputs from a deck of cards. A typical card
is defined by punching a zero in column 2. The field that covers
columns 5 - 20 is used by the user for any descriptive statements with
which he wishes to identify the input. Column 21 -25 contains the right-

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justified integer number of the tape transport to be used. The number of
the first record to be read is punched in column 31 - 45. The last
field is column 46 - 60 which contains the number of records to be read.
The last two fields may use either fixed or floating-point notation.

2. Type 1 Card

Type 1 cards are used to specify which operational subroutines
are called during the flight simulation. This type card is identified
by the number one in column 2. The second field is column 5 - 20 which
contains any identifying information. This information is printed out
when the data deck is read and allows the user to read exactly which
subroutines were called. Column 21 - 25 contains the right-justified
integer number which is the subroutine identifying number. The opera-
tional subroutine numbers are;

Subroutine	Subroutine Number
INPT1, INPT2, INPT3	2
OUPT1, OUPT2, OUPT3	3
STGE1, STGE2, STGE3	4
CNTR1, CNTR2, CNTR3	5
RNDM1, RNDM2, RNDM3	6
AUXA1, AUXA2, AUXA3	7
AUXB1, AUXB2, AUXB3	8
AUXC1, AUXC2, AUXC3	9

It should be noted that all or any of the subroutines listed under one
one number can be called by including only one card. The cards are
placed in the data deck in the order in which they will be called.
This order or sequencing will be explained further in section F,
Sequencing. A typical type 2 card is identified by the number two in

column 2. In general, column 5 - 20 should contain the module title, but any pertinent information is allowed. The module number is punched in column 21 - 25 and it must be right-justified. A listing of the module numbers follows:

Module	Module Number	Module	Module Number
A1,A1I	2	D4,D4I	20
A2,A2I	3	D5,D5I	21
A3,A3I	4	G1,G1I	22
A4,A4I	5	G2,G2I	23
A5,A5I	6	G3,G3I	24
C1,C1I	7	G4,G4I	25
C2,C2I	8	G5,G5I	26
C3,C3I	9	G6,G6I	27
C4,C4I	10	S1,S1I	28
C5,C5I	11	S2,S2I	29
C6,C6I	12	S3,S3I	30
C7,C7I	13	S4,S4I	31
C8,C8I	14	S5,S5I	32
C9,C9I	15	S6,S6I	33
C10,C10I	16	S7,S7I	34
D1,D1I	17	S8,S8I	35
D2,D2I	18	S9,S9I	36
D3,D3I	19	S10,S10I	37

Note that either the module, the initialization module, or both may be called by including only one card in the deck. A sample of a typical type 2 card is shown in Figure 3 (Ref. 7).

COLUMN

2	5	20	21	25			
2	MODULE 55			32			.

TYPICAL TYPE 2 CARD

FIGURE 3

2	5	20	21	25	31	45	46	60
3	WEIGHT			86	1152.0 — — — 1.152 E+03		1.0 — — — — 1.0 E+00	

TYPICAL TYPE 3 CARD

FIGURE 4

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4. Type 3 Card

Type 3 cards are used to set any COMMON(3415) location to any value other than zero. In general, four items must be initialized. The state variable initial values and any constants used in the flight simulation are the most obvious. Additionally, there are some constants associated with the executive programs and operational subroutines and the state variable upper and lower bounds which must be initialized. As with all cards, column 2 defines the type card and it must contain a three. Column 5 - 20 holds the statement describing the input. The user should be specific here since it will save him having to remember every COMMON(3415) location. The only other means of input identification is by column 21 - 25. These columns contain the right-justified COMMON location of the input. Columns 31 - 45 hold the actual numerical value of the input. The last field, column 46 - 60, contains the reset flag. If the reset flag equals one, the COMMON(3415) location and the numerical value are placed in the reset list. This list may contain up to fifty different variables. This, in the case of multiple runs, allows the variables to be reset to its initial value prior to each run without additional input cards. The sample card in Figure 4 (Ref. 8) shows that either fixed or floating-point notation may be used to input the numerical value and the reset flag. These cards need not be inputed in any specific order, but for ease of checkout, it is advised to place them sequencially by their COMMON location.

5. Type 4 Card

The MOD6DF program can printout a maximum of fifty variables for each simulation. Type 4 cards are used to specify which variables are to be printed. Column 2 must contain the number four to indicate a type

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4 card. When the results are printed out headings are included. These headings are designated in column 9 - 20. The exact alphanumeric title punched will be printed at the top of each page, this need not be the fortran symbol used within the program. The COMMON(3415) location of the output variable is contained in column 21 - 25 and must be right-justified.

6. Type 5 Card

Type 5 cards are used to indicate which variables are to be root-mean-squared. These cards are similar to type 1 and type 2 cards. Column 2 must contain the number five. Any pertinent information about the variable to be operated on is punched in column 5 - 20. The COMMON (3415) location of the variable must be right-justified in columns 21 - 25. The last field, column 31 - 45, indicates whether the root-mean-square operation will occur along the trajectory or at the end.

7. Type 6 Card

The type 6 card has two purposes. Its first function is trivial, but required. The number six is typed in column 2 and the rest is blank. This indicates to the computer program that there are no more input cards. Its second function involves random inputs. This card is used to indicate the number of random process (noise) generator cards that are to be read before the input process is terminated. Column 2 has the same information as before. Any pertinent information is contained in column 5 - 20. Columns 21 - 25 must be right-justified and they contain the number of random generator cards to be read.

E. AUXILIARY DECK

The auxiliary deck is a collection of subroutines and functions required by the modules. These routines are general in nature since

they can be called by several modules. They are used to calculate such things as the properties of air, engine performance, various ratios, and to locate values in the many data tables. A brief discussion of the most common subroutines is presented.

1. Boost

This subroutine calculates the thrust coefficient (CT) and the fuel flow rate (FF) during the boost phase. These values are returned to module A3 and used to calculate the missile thrust in the body axes and the missile weight.

2. Ramjet

This subroutine is used during the midcourse, cruise, phase of the missile flight. It uses a simplified ramjet model to calculate the thrust coefficient and fuel flow rate. This routine is not automatically called. The user must designate that he wishes to use it by inputing a type 3 card setting FLGRJ(606) equal to one. This then sets up the proper stepping in module A3.

3. Engine

This is the primary routine during the cruise phase. It is one of many routines within the NWC air-breathing propulsion package. This entire package is utilized to calculate the engine parameters from inlet to exhaust. Again, thrust coefficient and fuel flow rate are eventually computed and returned to module A3. The user does not need to supply any special input cards to use this subroutine. If no initial value is inputed for FLGRJ(606) it is automatically set to zero, which indicates this routine is to be used.

4. Air

All the properties associated with the air are calculated in

this subroutine. This includes the computation of the speed of sound and the dynamic pressure. Since the missile does vary in altitude, the routine takes this into account as well as the latitude. Once these values are calculated, they are returned to module G3.

5. Block Data

This routine contains data tables. These tables cover parameters from aerodynamic coefficients to thermal properties. The total data package covers specific bands within the missile operating envelope. Data is stored in matrices which includes one, two, and three dimensional ones. These data tables are readily available and there are routines designed to retrieve this information quickly.

6. Serch

This subroutine, along with several functions, is used to retrieve information from BLOCK DATA. If the present operating point of the missile is not within one of the bands of information, then the tables are interpolated. The functions THREDL, STDLI, STDLIA, and TAB do the interpolation of the tables. Since the tables are of various lengths, these functions are very general.

F. SEQUENCING

Sequencing is very important in the running of the MOD6DF program. Care must be taken to ensure that the modules are processed in the correct order at each step. This is essential to eliminate the use of obsolete values from the last cycle. An exception to this problem is the state variables. These are updated simultaneously by the integration algorithm. Any module is capable of using the most current value of these, no matter what the order of processing.

To help remedy this problem, module diagrams were devised. Module

diagrams aid the user in maintaining the proper flow of variables into and out of the modules. To design a module diagram start with a box. This box will contain all the equations for a specific module. The standard procedure for showing inputs and outputs is to use arrows pointing in or out from either the left or the right side. The example in Figure 5 (Ref. 9) shows this technique. The arrows pointing in from the left indicate variable inputs from other modules. Arrows pointing out to the right indicate output going to either other modules or program output. The last set of arrows points in from the right. These show the constants brought in directly or indirectly from the initialization module. Since each arrow represents a variable, they must be defined. The usual means of labeling the arrows is to use the variable fortran symbol and in parenthesis its COMMON(3415) location.

Each variable usually has only one COMMON location associated with it. In the case of 'state' variables this is not true. State variables are defined by four consecutive COMMON locations. The first is for the derivative of the variable. The second and the third locations hold the lower and upper bounds, respectively, of the integration error. The last one contains the variable itself.

Once all the required module diagrams have been completed, they can be combined to get the overall processing order. The usual processing order, shown in Figure 6 (Ref. 10) is to start with the geophysical group, then proceed to sensors, computers, airframe, and finally dynamics. Within each group is a usual processing order and this too is shown in Figure 6. This process for determining the program sequence will eliminate the use of any obsolete values in the computer run.

$$\dot{X}2 = Ak \cdot X1$$

X1(706) →

Ak(710) ←

$\dot{X}2$(711) →

ELX2(712) ←

EUX2(713) ←

X2(714) →

MODULE DIAGRAM
FIGURE 5

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PROCESSING SEQUENCE

FIGURE 6

IV. COMPUTER PROGRAM CHECKOUT

The basis for the research was the MOD6DF computer program from NWC China Lake. The total package received from them consisted of a listing of the program and an uninterpreted deck of cards. The initial step was to input the cards in small groups into the computer and then to examine the source listing. This listing revealed that the original deck was punched in BCD. This fact was easy to determine since several characters were changed (Ref. 11). The library routine NEWDEK was used to translate the cards from BCD to EBCDID.

Once the translation was completed, an attempt was made to compile the new deck. This produced an output which contained many syntax errors. These errors were divided into two major groups. One effected the use of quotation marks in FORMAT and comment statements. The other one, the more difficult, effected the DATA statements in the BLOCK DATA subroutine.

The problem with the DATA statements was due primarily to the difference in the compilers used. The compiler at NWC was much newer and allowed for the use of more sophisticated inputs. The compiler at NPS only allows a data set to start with the first element. This required the rewriting of many data groups. To complicate these revisions, a limit of nineteen continuation cards is also imposed. These restrictions demanded not only the rewriting of many data sets, but also the formation of two new ones.

With the corrections finally completed, the computer would then compile the program. The next step was to link all the subroutines together. The first attempt was unsuccessful. Inadvertently, the subroutine INTR20 had been omitted from the original deck. Using the program listing, the contents of INTR20 were typed and included in the

main deck. With this addition the program would now compile and link.

Now that the program would compile and link, attention was turned to getting a good simulation. To facilitate this process, two sample outputs were obtained from NWC. These outputs cover one missile flight which is broken down into a midcourse guidance and a terminal guidance s imulation. Hereafter these will be referred to as midcourse baseline and terminal baseline, respectively. Using the initial conditions from the baseline models, it was hoped that the outputs could be duplicated.

A. MIDCOURSE GUIDANCE FLIGHT

The initial run, using the midcourse baseline inputs, revealed an overflow problem with the dynamic pressure (QD(508)). Us ing the traceback procedures outlined in the Users Manual from the W. R. Church Computer Center, the problem was confined to subroutine AIR. The problem turned out to be a translation error. The symbol $P\emptyset$ ($\emptyset$ - zero) had translated to $P\emptyset$ in one place and PO in another. This error caused the program to use a value left in that memory location from a previous run to calculate the dynamic pressure. With this problem remedied, the program could progress a little farther. The next stumbling block appeared as a divide check. These errors were resolved by introducing patches that would bypass a statement that tried to divide by zero. Once bypassed, that quantity would be set equal to zero. This was the normal procedure of the computer, but it would stop the run after ten such errors. Having corrected all these errors, output was obtained which covered the desired seventy seconds of flight.

When the output was examined a major switching problem within sub-routine A3 (missile propulsion module) was found. The midcourse baseline utilized a simplified ramjet model, but the output was not.

ALTITUDE VS. TIME (MIDCOURSE)

FIGURE 7

ALTITUDE (kft)

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Rather than use RAMJET, the output disclosed that ENGINE had been used. The problem was in the logic statement, FLGRJ 0.0. The program was not making the desired switch to the simplified ramjet model. To remedy the problem, the data card FLGRJ(606) 1.0, was added to the input data deck. Another problem was discovered which occured between 14.0 and 14.5 seconds. During that time period the missile angle of attack (ALPHA (330)) exceeded ten degrees. When ALPHA exceeds this angle the engine is turned off. With the engine off, no thrust is produced causing the forward velocity (VXTP(286)) to decrease. This limitation was removed from the program. After eliminating these problems a flight trajectory, Figure 7, was obtained which closely resembled the output of the mid-course baseline. A random sampling of the outputed variables were compared for exactness. The differences noted were due primarily to computer round-off error.

To further verify the accuracy of the two simulations, three parameter (TXBA(073), VXTP(286),and YTP(298))were chosen as representative values for the runs. To obtain a feel for the run, these parameters are plotted in Figures 8, 9, 10. Additionally, random time samples are tabulated in Tables I, II, III.

The thrust (TXBA(073)) plot, Figure 8, can easily be divided into four mission phases. During the separation phase (0.0 - 4.5 seconds) the thrust is zero. This is expected since neither of the engines have ignited. This is followed by a rapid increase in the thrust. The maximum thrust, 27800 lbs, happens during the boost phase (4.5 - 9.5 seconds). At 9.5 seconds the boost motor stops and the transition phase occurs for the next 0.3 seconds. During this time the thrust decreases rapidly since neither engine is on. Once the engine port covers are

THRUST VS. TIME (MIDCOURSE)

FIGURE 8

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VXTP VS. TIME (MIDCOURSE)

FIGURE 9

VXTP (ft/s)

YTP VS. TIME (MIDCOURSE)

FIGURE 10

clear, the ramjet sustainer ignites. This action initiates the midcourse phase (9.8 - 70 seconds) and the thrust remains relatively constant at 1200 lbs.

The missile forward velocity (VXTP(286)) can be directly related to the thrust. During separation no thrust is produced, therefore the velocity is zero. As the missile is boosted to Mach two, the velocity increases and approaches its maximum value (2800 ft/s) just prior to boost engine shut-down. As the sustainer engine port covers clear, the velocity decreases slightly. Once the ramjet engine ignites the velocity profile is displayed in Figure 9 and it closely resembles that for the midcourse baseline.

The last parameter, y-displacement (YTP(298)), was included to demonstrate the accuracy of the guidance system Figure 10 shows that prior to attaining the cruise altitude, the missile wanders off track. Once the guidance system is activated, it makes the necessary corrections to return the missile to the planned flight path. Table III shows that the y-displacement corresponds to the baseline case and at the conclusion of the run the off-track error is down to 12.03 feet.

All the information obtained from the new run was checked against the midcourse baseline. The results showed that the two simulations are within acceptable limits. With this milestone completed, the program checkout could proceed to the terminal guidance flight.

B. TERMINAL GUIDANCE FLIGHT

To checkout the terminal guidance portion of the MOD6DF program, the initial conditions from the terminal baseline were used. This required changing about a dozen input cards in the midcourse input data deck. The first run attempted turned out successful. This was due to the

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TIME	0.0	7.5	10.0	20.0	25.5	30.0	40.0	50.0	60.0	70.0
BASELINE	0.0	27395	1140.6	1403.0	1377.4	1281.0	1211.3	1178.0	1148.1	1124.8
NEW	0.0	27391	1138.9	1514.3	1418.4	1314.3	1249.9	1207.0	1175.5	1149.7

TXBA (073) COMPARISON (MIDCOURSE)

TABLE I

TIME	0.0	7.5	10.0	20.0	25.0	30.0	40.0	50.0	60.0	70.0
BASELINE	681.99	1858.3	2790.2	2606.7	2604.9	2613.4	2652.4	2705.0	2743.8	2771.5
NEW	681.99	1851.7	2786.3	2506.4	2525.9	2544.5	2605.0	2665.5	2710.8	2743.9

VXTP (286) COMPARISON (MIDCOURSE)

TABLE II

TIME	0.0	7.5	10.0	20.0	25.0	30.0	40.0	50.0	60.0	70.0
BASELINE	-5E-5	3.46	11.37	27.21	25.92	24.34	20.45	16.93	13.24	9.39
NEW	-5E-5	3.19	10.68	24.43	23.93	22.82	21.96	19.14	15.81	12.03

YTP (298) COMPARISON (MIDCOURSE)

TABLE III

TIME	0	5.0	10.0	12.6	15.0	17.6	20.0	22.6	25.0	TF
BASELINE	1141.9	1131.0	1077.8	1170.9	1309.4	1501.1	1730.0	2245.3	2565.8	2691.3
NEW	1141.6	1134.8	1099.4	1212.8	1359.3	1561.7	1800.0	2305.9	2584.3	3273.6

TXBA (073) COMPARISON (TERMINAL)

TABLE IV

TIME	0.0	5.0	10.0	12.6	15.0	17.6	20.0	22.6	25.0	TF
BASELINE	2750.0	2764.2	2654.6	2471.4	2225.7	1854.5	1391.4	1376.9	1413.1	1425.05
NEW	2750.0	2761.5	2631.5	2438.7	2192.1	1828.2	1389.3	1366.7	1406.1	1465.2

VXTP (286) COMPARISON (TERMINAL)

TABLE V

TIME	0.0	5.0	10.0	12.6	15.0	17.6	20.0	22.6	25.0	TF
BASELINE	0.0	0.0	-.4E-6	-.5E-6	.7E-6	.9E-6	.1E-5	.2E-6	.1E-6	.1E-6
NEW	0.0	-.0074	.019	-1.38	-.095	-.868	-1.77	.071	-.151	-.05

YTP (298) COMPARISON (TERMINAL)

TAVLE VI

ALTITUDE VS. TIME (TERMINAL)

FIGURE 11

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elimination of all the errors during the midcourse checkout. The result-

ing flight trajectory, Figure 11, is a very good illustration of the

desired profile. To check the accuracy of the simulation, the same

three parameters were chosen. Tables IV and V show that this run is

almost identical to the terminal baseline. The difference is primarily

due to computer round-off error. Figures 12 and 13 show the overall

flight performance of the thrust and forward velocity, respectively.

For this simulation, the y-displacement (YTP(298)) does not

compare favorably with the terminal baseline. Figure 14 shows that be-

tween ten and twenty seconds in the flight, YTP develops rapid

oscillations. By examining Table VI, it is noted that during this

interval the two simulations differ the most. No reason for this

discrepancy could be found. These oscillations do effect the flight by

increasing the time of flight from 25.825 to 29.09 seconds and by

increasing the miss distance. The imposed time constraints force this

problem to be overlooked and to direct attention to the accuracy of the

impact. Since the impact is within 0.5 feet of the target location, it

is concluded that the terminal guidance simulation works properly.

With both segments of the MOD6DF computer program working correctly,

thoughts could now turn towards the actual experimental runs. The

results of these runs are discussed in the next section.

THRUST VS. TIME (TERMINAL)

FIGURE 12

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VXTP VS. TIME (TERMINAL)

FIGURE 13

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YTP VS. TIME (TERMINAL)

FIGURE 14

55

V. TERMINAL FLIGHT DISTURBANCES

With the checkout of the MOD6DF computer program completed, many ideas were discussed concerning alterations to the simulations. The three modifications decided upon were:

* examine target miss distance when changes were made to the initial x-y-z conditions,

* examine the terminal flight profile, range, and miss distance when the cruise altitude was reduced to approximate a sea skimming mode,

* examine target miss distance when random noise is applied to the missile homing seeker.

To understand the changes and results, one must be familiar with the frame of reference. The origin of the reference frame travels from the launch platform to the target location at the cruise altitude. This is called the tangent plane reference system. Displacements in the x-direction (XTP(290)) are measured from the launch platform in the direction of the target. Y-displacements (YTP(298)) are measured left or right of the ideal flight path, in the tangent plane. Any vertical displacement (ZTP(306)) is measured normal to the ideal flight path, with down being the positive direction. Using this frame of reference the information in Table VII is easier to understand.

The first modifications demonstrate the effect of changing YTP. YTP was increased until a result was reached that was unsatisfactory. From the results in Table VIII, the maximum value of YTP was determined to be 1800 feet. This conclusion corresponds with the results in reference 13. Since the missile is symmetric, it was also concluded that moving YTP either right or left would give the same results.

The fifth run simulated a drop in the missile's altitude. ZTP was

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RUN	XTP	YTP	ZTP
BASELINE	1735552.5	0.0	0.0
1	173552.5	1000.0	0.0
2	173552.5	1500.0	0.0
3	173552.5	1800.0	0.0
4	173552.5	2000.0	0.0
5	173552.5	0.0	2000.0

INITIAL CONDITIONS

TABLE VII

RUN	XTP	YTP	ZTP	IMPACT TIME
BASELINE	234999.56	-.0506363	34999.34	28.825
1	234999.81	.1259258	34999.836	29.108
2	235000.19	.11479032	35000.32	29.124
3	235000.25	.15263242	35000.391	29.134
4	269802.0	2000.0	19705.00	35.0
5	234999.63	.45691	35000.428	30.365

IMPACT RESULTS

TABLE VIII

inputed as 2000.0 feet. As the simulation progressed, the missile

developed the necessary commands to climb and regain the desired cruise

altitude (Figure 15). It then commenced its terminal dive. The target

was detected, acquired, and impact followed. This initial condition

modification produced the largest miss distance (0.457 ft.).

Figure 16 was presented to show the relative locations of the miss

distances for each change. Table VIII reveals that up until 1800 feet,

changes to YTP created very little variation in the miss distance. It

should be noted that the larger the displacement became, the greater the

time until impact. The increase in time was necessary to allow the

missile to acquire the target and then compute the required acuator

commands to impact the target. This concluded the investigation of the

effects of initial displacement error on target miss distance.

The idea behind changing the cruise altitude was to try and simulate

a sea skimming profile. RAMJET contains tables that allow for four

cruise altitudes. Of these four altitudes, the lowest (500 ft) was

chosen even though it is high for a sea-skimmer. To run this simulation

only two input data card changes were required. HO(414) and HREF(501)

had to be set equal to the desired altitude. The resultant flight path

is shown in Figure 17.

The simulation produced an error-free output, but at first glance

the results appeared unacceptable. Still trying to compare miss dis-

tances, the downrange distance (XTP) was found to be 197916 feet.

Comparing this to the terminal baseline (234999) resulted in an extreme

error. It was then realized that the missile must expend more fuel at

this altitude to attain the same speed. Therefore, the results could be

correct. As further verification of the correctness of the run, it was

assumed that the missile weight at impact should be fairly equal. The

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ALTITUDE VS. TIME (TERMINAL - ZTP)

FIGURE 15

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YTP(ft)

235000.4

234999.6

XTP (ft)

BASELINE

△5

△3

△2

△1

ORIGIN:
XTP=235,000
YTP=0.0

IMPACT RESULTS

FIGURE 16

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ALTITUDE VS. TIME (SEA-SKIMMER)

FIGURE 17

62

simulation impact weight was 1126.34 lbs while the terminal baseline weighed 1113.12 lbs. Since no conflicting information could be found in reference 12, it was concluded that this simulation was correct.

The final flight disturbance investigated was the addition of random noise to the missile homing seeker. This simulation proved to be unsuccessful due to invalid input format. The information describing the process is brief and difficult to understand. Further information from NWC China Lake is required to be able to successfully run simulations with random noise.

With the completion of these modifications, many unanswered problems and questions still exist. The two most critical problems concern the input of random noise generators and the missile exceeding the angle of attack limitation when using ENGINE for cruise propulsion. However, the simulations did show that the MCD6DF program runs correctly at alternate cruise altitudes and with initial displacement errors.

VI. CONCLUSION

The MOD6DF computer program from NWC China Lake was converted to operate on the IBM-360 computer at the Naval Postgraduate School. The program would only function properly when using the simplified ramjet model. When this model was not used, the missile angle of attack exceeded the maximum limit of ten degrees. This error caused the ramjet engine to flame out.

Target impact errors for the terminal guidance problem were investigated when the initial displacement was modified. These modiifications demonstrate the missile's accuracy when removed from the ideal flight path. The results also point out that if the target falls within the seeker search pattern, target impact will inevitably happen.

Random noise generation is possible with the MOD6DF program. However, more information discussing the parameters required to develop the noise is necessary. Additionally, sample noise inputs should be obtained that reflect the alteration to the noise subroutines.

This research involved the preliminary investigation of the MOD6DF program. The program has many possible areas, concerning guidance and control of tactical missiles, which could be developed for future study. These areas not only include the unresolved problems encountered during this research. Additionally, reference 14 and 15 contain many examples of possible advanced guidance concepts.

COMPUTER OUTPUT

TIME THRUST WEIGHT X(TP) X(FP)

G ALT Y(TP) VX(F)

F VELOCITY Z(TP) VZ(FP)

P PITCH ALPHA(CEG) ALFA(DEG)

ANYC ANACH DELTA G(DEG) DELTA F(DEG)

TALFT MARGIN GYN R YAW (RAD)

0.46559950E-02

0.20999952E 00

0.40499951E 00

0.60499984E 00

0.80499983E 00

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```
C     THIS IS THE MAIN NCD6CF PROGRAM
      COMMON C(3415), TEMPS(1500)
      EQUIVALENCE (C(3415),A)
      EQUIVALENCE (C(2911),HMIN)
      EQUIVALENCE (C(2912),HMAX)
      EQUIVALENCE (C(2914),DER(1))
      EQUIVALENCE (C(2915),VAR(1))
      EQUIVALENCE (C(3215),EL(1))
      EQUIVALENCE (C(3216),T)
      EQUIVALENCE (C(2904),KSTEP), (C(2905),STEP)
      EQUIVALENCE (C(2907),LSTEP)
      DIMENSION IPL(101)
      DIMENSION DER(100)
      DIMENSION VAR(100)
      DIMENSION EU(100)
      N=M
      CALL ZERO
      CALL CINPT1,STEP
      LSTEP = VSEL1
      CALL AUXH1
      CALL SUBL2   2,N
60    DO 60 I=1,N
      IPL(I-1) = C(J+1)
      VAR(I-1) = C(J+2)
      DER(I-1) = C(J+3)
      CALL AUXSUB
      ANK = AI
      DO 50 I=1,N
      VAR(I-1) = VAR(I) + VAP(I)
50    C(J+3) = VAR(I-1)
      CALL VSEL3
      IF(KSTEP .EQ. 1) GO TO 1007
      IF(KSTEP-1) 70,1007,7C
1005  CALL PROCES
70    CALL RESET
      GO TO (1000,1001,10C2,1003,1004,1005,1006,1C07,1008,1009,1010),
```

```
      1 LSTEP
 1010 CALL EXIT
      STOP
      END

C
C
      SUBROUTINE ZERO
C
      COMMON C(3415)
      DO 1 KLEAR = 1, 4915
    1 C(KLEAR) = 0.0
      RETURN
      END

C
C
      SUBROUTINE OINPT1
C
C  BASIC INPUT SUBROUTINE OINPT1
C  SUBROUTINE OINPT1 IS THE BASIC INPUT SUBROUTINE
C
      DIMENSION LISTNO(50), VALUE(50)
      DIMENSION SUBNO(99), IR(2), VR(2)
      DIMENSION RACMNO(50)
      DIMENSION ALPHA(4), CNAME1(50), ONAME2(50), ONAME3(50), OUTNO(50)
      DIMENSION MCCNO(99)
      DIMENSION STATNO (100)
      COMMON C(3415)
      REAL C, OUTNO
      INTEGER RACMNO
      INTEGER STATNO
      EQUIVALENCE (C(2442), LOSTAT)
      EQUIVALENCE (C(2201), STATNO(1)), (C(2441), NOSTAT),
     1             (C(2801), NOSUB), (C(2802), SUBNO(1)), (C(2663), IR(1)),
      EQUIVALENCE (C(2661), VR(1))
      EQUIVALENCE (C(2701), NCMOD)
      EQUIVALENCE (C(2661), NCOUT)
      EQUIVALENCE (C(2448), NORNDM )
      EQUIVALENCE (C(2300), NOLIST), (C(2301), LISTNO(1)), (C(2351),
     1             (C(2500)  ,  OUTNO(1))
      EQUIVALENCE (C(2550)  ,  CNAME1(1))
      EQUIVALENCE (C(2600)  ,  ONAME2(1))
      EQUIVALENCE (C(2150)  ,  ONAME3(1))
      EQUIVALENCE (C(2445)  ,  RADMNO(1))
      EQUIVALENCE (C(2702), MCCNO(1))
      JAR = C
```
```
                                                    MCC60530
                                                    MCC60540
                                                    MCC60545
                                                    MCC60550


                                                    CINP0003C
                                                    CINP0001C
                                                    CINP0002C

                                                    CINP0023C
                                                    CINP0024C
                                                    CINP0025C

                                                    CINP0030C
                                                    CINP0040C
                                                    CINP0031C
                                                    CINP0032C
                                                    CINP0034C
                                                    CINP0005C

                                                    CINP0011C
                                                    CINP0012C
                                                    CINP0013C


                                                    CINP0035C
```

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```
      1 READ(5,2) IR(1),ALPHA(1),ALPHA(2),ALPHA(3),ALPHA(4),IR(2),VR(1),
     1 VR(2),                      IR(1),ALPHA(1),ALPHA(2),ALPHA(3),ALPHA(4),IR(2),VR(1),
     1 WRITE(6,2) IR(1),ALPHA(1),ALPHA(2),ALPHA(3),ALPHA(4),IR(2),VR(1),
     1 VR(2),
      2 FORMAT(I2,2X,4A4,I5,5X,2E15.8)
        IF (IR(1).NE.0) GO TO 7
     18 I1=IR(2)          7,18,7
        I2 = VR(1) - 1.
        REWIND I1
        I3 = VR(2)
        IF (I2) 11,15,14
     14 DO 8 I1,10) J,X
      8 READ (I1,3) J,X
     15 READ (I1,2) J,X
    C   C(J) = X
     10 FORMAT (I5,E15.9)
     11 JAR = 1
        GO TO 1
    C
      7 IF (IR(1).NE.1) GO TO 3
      7 IF (IR(1)-1) 3,19,3
     15 NOSUB = NCSUB + 1
        SUBNO(NCSUB) = IR(2)
    C
      3 IF (IR(1).NE.2) GO TO 4
     20 IF (IR(1)-2) 4,20,4
        NOMOD = NCMOD + 1
        MODNO(NCMOD) = IR(2)
        GO TO 1
    C
      4 IF (IR(1).NE.3) GO TO 5
     21 IF (IR(2)-3) 5,21,5
        L = C(L)
        IF (JAR.EG.1) WRITE (I1,10)L,VR(1)
     22 IF (JAR-1) 23,22,23
     23 WRITE (I1,10)L,VR(1)
     24 IF (VR(2).EQ.0.) GO TO 1
        NOLIST = NOLIST + 1
        LISTAC(NCLIST) = L
        VALUE(NCLIST) = VR(1)
        GO TO 1
    C
      5 IF (IR(1).NE.4) GO TO 6
     25 IF (IR(1)-4) 6,25,6
        NOCUT = NCCUT +1
        CNAME1(NCCUT) = ALPHA(2)
```

```
      CNAME2(NOCUT) = ALPHA(3)                                    CINP1150
      CNAME3(NOCUT) = ALPHA(4)                                    CINP1160
      CUTNO(NOCUT) = IR(2)                                        CINP1170
      GO TO 16                                                    IINP1200
    6 IF (IR(1) .NE. 5) GO TO 16                                  CINP1210
      IF (IVR(1) - 5) 16,26,16                                    CINP1220
   26 IF (IVR(1) - 27,17,27) GO TO 17                             CINP1230
   27 LCSTAT = LCSTAT + 1                                         CINP1240
   17 NOSTAT = NOSTAT + 1                                         CINP1250
      STATNO(NOSTAT) = IR(2)                                      CINP1260
      GO TO 16
C
   16 NORNOM=0                                                    CINP1310
      IF (IR(2).EQ.0) RETURN                                      CINP1320
   28 IF (IR(2)) 29,28,29                                         CINP1330
   29 RETURN
C
      DO 12 I = 1 , N                                             CINP1370
   13 READ (5,13) J,Y,ZSTART,SIGNO,BETA                          CINP1400
      WRITE(6,13) J,Y,ZSTART,SIGNO,BETA                          CINP1410
   13 FORMAT(I5,2F5.0,3E15.9)
      NORNOM(I) = J
      RNOMNO(I) = J                                               CINP1440
      CC(J+1) = ZSTART                                            CINP1450
      CC(J+3) = SIGNO                                             CINP1460
   12 CC(J+4) = BETA                                              CINP1470
      RETURN
      END

      SUBROUTINE  SUBL1                                           SUBL0010
C                                                                 SUBL0020
CCC   COMMON C(3415)                                              SUBL0050
C     DIMENSION  SUBNO(95)                                        SUBL0030
      EQUIVALENCE (C(2801),NOSUB)
      EQUIVALENCE (C(2802),SUBNO(1))                              SUBL0060
      DO 1 I=1,NOSUB                                              SUBL0070
    1 GO TO SLENO(I)                                              SUBL0100
    2 CALL INFT1, 2, 3, 4, 5, 6, 7, 8, 9 1, J                     SUBL0120
    3 GO TO CUPT1                                                 SUBL0130
    3 CALL CUPT1                                                  SUBL0140
    4 GO TO SIGE1                                                 SUBL0150
    4 CALL SIGE1                                                  SUBL0160
    5 GO TO CNTF1                                                 SUBL0170
    5 CALL CNTF1
```

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```
6     GO TO 1
      CALL RACM1                                                  SUBL020C
7     GO TO 1                                                     SUBL021C
      CALL ALXA1                                                  SUBL023C
8     GO TO 1                                                     SUBL024C
      CALL ALXB1                                                  SUBL025C
9     GO TO 1                                                     SUBL026C
      CALL ALXC1                                                  SUBL027C
1     CONTINUE                                                    SUBL031C
      RETURN                                                      SUBL031C
      END                                                         SUBL032C

      SUBROUTINE  SUBL2                                           SUBL0010

      DIMENSION SUBNO(99)                                         SUBL0050
      COMMON C(3415),ACSUB                                        SUBL002C
      EQUIVALENCE (C(2801),ACSUB)                                 SUBL003C
      EQUIVALENCE (C(2802),SUBNO(1))
      DO 1 SUBNO(I) = ACSUB                                       SUBL006C
      J = SUBNO(I)                                                SUBL007C
      GO TO (1, 2, 3, 4, 5, 6, 7, 8, 9), J                        SUBL010C
2     CALL INFT2                                                  SUBL011C
      GO TO 1                                                     SUBL012C
3     CALL CLFT2                                                  SUBL014C
      GO TO 1                                                     SUBL016C
      CALL STGE2                                                  SUBL017C
4     CALL CNTR2                                                  SUBL021C
      GO TO 1                                                     SUBL023C
5     CALL RACM2                                                  SUBL024C
      GO TO 1                                                     SUBL025C
6     CALL ALXA2                                                  SUBL026C
      GO TO 1                                                     SUBL027C
7     CALL ALXB2                                                  SUBL030C
      GO TO 1                                                     SUBL031C
8     CALL ALXC2                                                  SUBL032C
      GO TO 1
1     CONTINUE
      RETURN
      END

      SUBROUTINE  SUBL3                                           SUBL0010

      DIMENSION SUBNO(99)                                         SUBL0050
      COMMON C(3415)                                              SUBL002C
```

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```
      EQUIVALENCE (C(2801),NOSUB)
      EQUIVALENCE (C(2802),SUENO(1))
      DO 1 I=1,NOSUB
      J = SUENO(I)
      GO TO (1,2,3,4,5,6,7,8,9),J
    2 CALL INFT3
      GO TO 1
    3 CALL CLFT3
      GO TO 1
    4 CALL STCE3
      GO TO 1
    5 CALL CATF3
      GO TO 1
    6 CALL RACN3
      GO TO 1
    7 CALL ALXA3
      GO TO 1
    8 CALL ALXB3
      GO TO 1
    9 CALL ALXC3
    1 CONTINUE
      RETURN
      END
```

```
      SUBROUTINE AUXI
      DIMENSION MCDNO(99)
      COMMON MCDNO(3415)
      REAL MCDNO
      EQUIVALENCE (C(2701),ACMOD)
      EQUIVALENCE (C(2702),MCDNO(1))
      EQUIVALENCE (C(2659),CNCE)
      EQUIVALENCE (C(3315),N)
      NCNCE = 0
      DO 1 I=1,NCNCD
      NCNC(I)=0
    1 NCNC(I)=0
      L = 0
      GO TO (1,2,3,4,5,6,7,8,9,10,11,12,13,14,15,16,17,18,19,20,21,22,23
     24,25,26,27,28,29,30,31,32,33,34,35,36,37),L
    2 CALL AI1
      GO TO 1
    3 CALL A2I
      GO TO 1
    4 CALL A3I
      GO TO 1
```

```
   29 CALL S2I
   30 CALL S3I
      GO TO 1
   31 CALL S4I
      GO TO 1
   32 CALL S5I
      GO TO 1
   33 CALL S6I
      GO TO 1
   34 CALL S7I
      GO TO 1
   35 CALL S8I
      GO TO 1
   36 CALL S9I
      GO TO 1
   37 CALL S10I
    1 CONTINUE
      RETURN
      END

      SUBROUTINE AUXSUB
      DIMENSION DER(101)
      DIMENSION VAR(101)
      DIMENSION IPL(100)
      DIMENSION MCDNO(99)
      COMMON MCDNO (415)     CC(2701),NOMOD)
      REAL MCDNO              CC(2702),MCDNO(1))
      EQUIVALENCE (CC(3316),IPL(1))
      EQUIVALENCE (CC(3014),VAR(1))
      EQUIVALENCE (CC(2916),DER(1))
      EQUIVALENCE (CC( 93),T)
      EQUIVALENCE (CC(3315),N)
      DO 5 I=1, N
      CC(J+3)=VAR(I)
   50 CC(J+3)=VAR(I)
      DO 1 MCDNC(I)=NCCE
      GO TO (1,2,3,4,5,6,7,8,9,10,11,12,13,14,15,16,17,18,19,20,21,22,
     123,24,25,26,27,28,29,30,31,32,33,34,35,36,37),L
    2 CALL A1
      GO TO 1
```

```
27  CALL G6                                              ALXS1110
    GO TO 11                                             ALXS1120
28  CALL S1?                                             ALXS1130
    GO TO 5?                                             ALXS1140
29  CALL S2?                                             ALXS1150
30  GO TO 3?                                             ALXS1160
31  CALL S4?                                             ALXS1170
    GO TO 11                                             ALXS1210
32  CALL S5?                                             ALXS1220
    GO TO 11                                             ALXS1230
33  CALL S6?                                             ALXS1240
    GO TO 11                                             ALXS1250
34  CALL S7?                                             ALXS1260
    GO TO 11                                             ALXS1270
35  CALL S8?                                             ALXS1310
    GO TO 11                                             ALXS1320
36  CALL S9?                                             ALXS1330
    GO TO 5?                                             ALXS1340
37  CALL S10?                                            ALXS1350
1   CONTINUE                                             ALXS1370
    J=IFL(I-1)?                                          ALXS1400
60  DO 60 I=2,N                                          ALXS1410
    DER(I) = C(J)                                        ALXS1420
    RETURN                                               ALXS1430
    END

    SUBROUTINE AMRK                                      AMRK0010
C   DOUBLE PRECISION VERSION, SAVES FUNCTION VALUES AND  AMRK0020
C   THE INDEPENDENT VARIABLE IN FULL D.P.                AMRK0030
                                                         AMRK0040
    DIMENSION V(1),D(1),FU(1),FL(1)                      AMRK0050
    DOUBLE PRECISION P1,P2,P3,P4,C2,C3,C4                AMRK0170
    DOUBLE PRECISION T(1:60),TME,DELT                    AMRK0210
    COMMON (3414) ,V(1)
    EQUIVALENCE (2915), ONCE                             AMRK0110
    EQUIVALENCE (3215), FL(1)                            AMRK0140
    EQUIVALENCE (2615), HMAX)                            AMRK0150
    EQUIVALENCE (2912), HMIN)                            AMRK0160
    EQUIVALENCE (2911)
    EQUIVALENCE (J1,NI)
```

```
      IF (CNCE) 2,1,2
    1 CNCE = 1.                                                          ARK0220
      CPT = 0.                                                           ARK0240
      P1 = .25                                                           ARK0260
      P2 = .4...1666666667                                              ARK0270
      P3 = ...3333333333                                                ARK0300
      P4 = .75...1666666667                                             ARK0310
      C2 = .2...6666666667                                              ARK0320
      C4 = .41666666667                                                 ARK0340
      KOUNT = 0                                                          ARK0350
      N = N1                                                             ARK0360
      J1 = J1                                                            ARK0370
      J2 = J2                                                            ARK0400
      J3 = J3                                                            ARK0410
      J4 = J4                                                            ARK0420
      J5 = J5                                                            ARK0430
      J6 = J6                                                            ARK0440
      J7 = J7                                                            ARK0450
      J8 = J8                                                            ARK0460
      J9 = J9                                                            ARK0470
      J10 = J10                                                          ARK0500
      J11 = J11                                                          ARK0510
      J12 = J12                                                          ARK0520
      J13 = J13                                                          ARK0530
      J14 = J14                                                          ARK0540
      IF (COPT) 60,49,60                                                 ARK0550
      IF (DELT .EQ. 0.) GO TO 60                                         ARK0560
      IF (DELT - (0.5*D(1))) 50,200,50                                   ARK0570
      KOUNT = 0                                                          ARK0600
C                                                                        ARK0610
C                                                                        ARK0620
   50 IF (COPT - (0.5*D(1))) 50,200,50                                   ARK0630
C     START RUNGE-KUTTA INTEGRATION.                                     ARK0640
C     COMPUTE K0                                                         ARK0650
C                                                                        ARK0660
   60 CONTINUE                                                           ARK0670
      DO 25 I=1,N1                                                       ARK0700
      K5=J15+I                                                           ARK0710
      IF(SNGL(T(K5)) .NE. V(I+1))T(K5) = V(I+1)                          ARK0720
      T(K5)=SNGL(V(I+1)) -V(I+1)) 24,25,24                               ARK0730
   24 CONTINUE                                                           ARK0740
   25 CONTINUE                                                           ARK0750
      IF(SNGL(TME) .NE. V(1)) TME = V(1)                                 ARK1000
   26 TMF=V(1)                                                           ARK1010
   27 KOUNT = KOUNT + 1                                                  ARK1020
   70 DO 80 I=1,N1
      K0=J7+I
```

```
80 T(KO)=C(1)*D(I+1)
C
C    COMPUTE K1
C
      DELT=C.5*C(1)
      TME=DELT+TME
      V(1)=TME
      DO 90 I=1,N1
      KO=J7+I
      K2=J1C+I
      K3=J13+I
      K5=J1?+I
      T(K1)=T(K2)
      T(K2)=T(K3)
      T(K3)=T(K5)
      T(K5)=T(K5)  +0.5*T(KO)
      V(I+1)=T(K5)
      CALL ALXSLB
90    DO 10C I=1,N1
      K1=J8+I
100   T(K1)=C(1)*D(I+1)
C
C    COMPUTE K2
C
      DO 110 I=1,N1
      K5=J15+I
      K1=J8+I
      KO=J7+I
      T(K5)=T(K5)  +0.5*(T(K1)-T(KO))
      V(I+1)=T(K5)
      CALL ALXSLB
      DO 120 I=1,N1
      K2=J9+I
120   T(K2)=C(1)*C(I+1)
C
C    COMPUTE K3
C
      TME=DELT+TMF
      V(1)=TME=TME
      DO 130 I=1,N1
      K5=J15+I
      K2=J9+I
      K1=J8+I
      T(K5)=T(K5)  +T(K2)-0.5*T(K1)
      V(I+1)=T(K5)
130   CALL ALXSLB
```

ARK1030C
ARK1040C
ARK1050C
ARK1060C
ARK1070C
ARK1100C
ARK1110C
ARK1120C
ARK1130C
ARK1140C
ARK1150C
ARK1160C
ARK1170C
ARK1200C
ARK1210C
ARK1220C
ARK1230C
ARK1240C
ARK1250C
ARK1260C
ARK1270C
ARK1300C
ARK1310C
ARK1320C
ARK1330C
ARK1340C
ARK1350C
ARK1360C
ARK1370C
ARK1400C
ARK1410C
ARK1420C
ARK1430C
ARK1440C
ARK1450C
ARK1460C
ARK1470C
ARK1500C
ARK1510C
ARK1520C
ARK1530C
ARK1540C
ARK1550C
ARK1560C
ARK1570C
ARK1600C
ARK1610C
ARK1620C

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```
      DO 140 I=1,N1
  140 T(K3)=C(1)*D(I+1)
C
C     COMPUTE VALUE OF FUNCTION.
C
      DO 150 I=1,N1
      K0=J7++I
      K1=J8++I
      K2=J9++I
      K3=J10++I
      K5=J11++I
      T(K5)=T(K5)+0.16666666667*
     1(T(K0)+T(K1)+T(K1)-4.*T(K2)+T(K3))
      V(I+1)=T(K5)
  150 CONTINUE
  170 CONTINUE
      CALL AUXSUB
      DO 180 I=1,N1
      K5=J1++I
      K0=J2++I
      K1=J3++I
      K2=J4++I
      K3=J5++I
      K4=J6++I
      T(K4)=T(K3)
      T(K3)=T(K2)
      T(K2)=T(K1)
      T(K1)=T(K0)
      T(K0)=T(K5)
      T(K5)=T(I)
      T(I)=T(I+1)
  180 CONTINUE
  190 CONTINUE
      RETURN
C
C     DO ADAMS-MOULTON INTEGRATION
C
  200 CONTINUE
      IF(KCUNT .LT. 3) GO TO 60
      IF(KCUNT - 3) 60,201,201
  201 KOUNT = KCUNT + 1
      DELT=C(1)*.5
      DO 210 I=1,N1
      K0=J7++I
      K1=J2++I
      K2=J3++I
      K4=J1++I
```

```fortran
      K5=J15+I
C
C COMPUTE Y-PREDICTED.
C
  210 T(KO)=T(K5)
      T(K5)=T(KO)+C(I)*(P1*T(I)-P2*T(K4)+P3*T(K1)-P4*T(K2))
      V(I+1)=TIME+C(I)
      TIME=TIME+C(I)
      V(I)=ALXSLB
      CALL ALXSLB
      K5=0
      DO 220 I=1,N1
      KO=J6+I
      K2=J7+I
      K1=JT+I
      K4=J15+I
      K3=J15+I
C
C COMPUTE Y-CORRECTED
C
      T(KO)=T(K1)+D(I)*(P4*D(I+1)+C2*T(I)-C3*T(K4)+T(K2)*C4)
      ERF=14.*DMAX1(DABS(T(K1)),.01D0)
      ERU=ERF*EL(I)
      ERL=ERF*EL(I)
      TEMF=DABS(T(KO)-T(K2))
      IF(TEMF-ERU)215,214,214
  214 IF(ABS(DELT).GE.+MIN) GO TO 260
  215 IF(ABS(DELT) - HMIN) 215,260,260
  216 IF(TEMF-ERL)216,220,220
  220 CONTINUE
C
      IF(K5 .LT. N1) GO TO 300
      IF(K5 - N1) 300,221,221
      IF(ABS(C(I)) .GT. HMAX) GO TO 300
      IF(ABS(D(I)) - HMAX) 222,222,300
C
C SET-UP FOR DOUBLING STEP SIZE
C
      IF(KCUNT .LE. 6) GO TO 300
      IF(KCUNT - 6) 300,300,221
  222 CONTINUE
  223 DO 240 I=1,N1
      K1=J1+I
      K2=J2+I
      K3=J3+I
```

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```
      K5=J5+I
      T(I)=T(K1)
      T(K1)=T(K2)
      T(K2)=T(K5)
      C(1)=C(1)+C(1)
      KOUNT=4
      DELT=.5*C(1)
      GO TO 200
C
C     SET-UP FOR HALVING STEP SIZE.
C
  260 CONTINUE
      IF(KOUNT .LE. 4) GO TO 350
      IF(KOUNT - 4) 350,350,261
  261 TME=TME-C(1)
      V(1)=TME
      C(1)=DELT
      DELT=.5*C(1)
      DO 265 I=1,N1
      K0=J7+I
      K1=J14+I
      K2=J9+I
      K3=J15+I
      K5=J15+I
      V(I+1)=T(KC)
      T(K3)=T(K2)+0.5*(T(K1)-T(K2))
      T(K2)=T(K1)+0.5*(T(I)-T(K1))
      T(K1)=T(I)
      KOUNT=4
      GO TO 200
  265 CC
C
C     INTEGRATION IS FINISHED. SET UP DERIVATIVES AND EXIT.
C
  300 DO 310 I=1,N1
      K5=J15+I
      K0=J8+I
      T(K5)=T(K0)
      V(I+1)=T(KC)
      GO TO 170
  310 CONTINUE
  350 CONTINUE
C
C     RETURN TO 3RD RK INTEGRATION AND RESTART
C
      DO 360 I=1,N1
      K5=J15+I
      K1=J11+I
      T(K5)=T(K1)
```

```
36C   V(I+1)=T(K1)                                                       APRK3770
      TME=TME-C(I)*4.                                                    APRK4000
      V(1)=TME                                                           APRK4010
      D(1)=CELT                                                          APRK4020
      CALL ALXSUB                                                        APRK4030
      GO TO 50                                                           APRK4040
      END                                                                APRK4050

C
C
C
      SUBROUTINE PROCES
      RETURN
      END

C
C
C
      SUBROUTINE RESET
      COMMON C(3415),(C(2300),NOLIST),(C(2301),LISTNO(1)),(C(2351),     INPT0010
     1 VALUE(1))  EQUIVALENCE  (C(2675),KRUN)
      DIMENSION LISTNO(50), VALUE(50)
      IF(NOLIST.EQ.0) RETURN
      DO 1 I=1,NOLIST
      J=LISTNO(I)
    1 C(J)=VALUE(I)
      KRUN=KRUN+1
      RETURN
      END

C
C
C
C
      SUBROUTINE INPT1                                                   F  96
      COMMON C(3415)
      COMMON/CRLS/MCNT/ENG/IENG(30),IENG(15)
      NAMELIST/MCNT/ENG,IENG
      EQUIVALENCE (C(2675), KRUN)
      FLG1=0.0                                                           F 106
      IF(KRUN.GT.0) GO TO 100                                           F 108
      READ(5,MCNT)
  10C WRITE(6,MCNT)
      RETURN
      END

C
C
      SUBROUTINE INPT2                                                   INPT0010
```

```
      RETURN                                                            INPT002C
      END                                                               INPT003C

      SUBROUTINE INPT3                                                  INPT001C
      RETURN                                                            INPT002C
      END                                                               INPT003C

      SUBROUTINE OUPT1                                                  OUPT001C
      RETURN                                                            OUPT002C
      END                                                               OUPT003C

      SUBROUTINE OUPT2                                                  OUPT002C

C     OUTPUT INITIALIZATION SUBROUTINE OUPT2                            OUPT001C

      COMMON C(3415)                                                    OUTP003C
      INTEGER PCCNT,DTCNT                                               OUTP013C
      EQUIVALENCE (C(2660),DTCNT)                                       OUTP004C
      EQUIVALENCE (C(2661),NCOUT)                                       OUTP005C
      EQUIVALENCE (C(2662),PCCNT)                                       OUTP006C
      EQUIVALENCE (C(2667),ITCNT), (C(2668),PCNT),(C(2669),CPP)         OUTP007C
      EQUIVALENCE (C(2670),TAPE), (C(2671), TAPENO)                     OUTP010C
      EQUIVALENCE (C(2909),CCC)                                         OUTP011C
      EQUIVALENCE (C(2910),KCCNV)                                       OUTP012C
      KCCNV = C                                                         OUTP014C
      ITCNT = C + 1.0                                                   OUTP015C
      PCNT  = C                                                         OUTP016C
      PGCNT = 1                                                         OUTP017C
      DTCNT = (NOCLT + 4)/5                                             OUTP020C
      IF (ITCNT .GE. 7) GO TO 2                                         OUTP021C
      IF (ITCNT .EQ. 7) 1,2,2                                           OUTP022C
   1  WRITE(6,6) (I=1,C(I),C(I+1),C(I+2),C(I+3),C(I+4),C(I+5),C(I+6),   OUTP023C
     1FORMAT(1H ,I5,2X,8F14.7))                                         OUTP024C
      TAPENO = C.                                                       OUTP025C
   2  K = TAPENO                                                        OUTP026C
      IF (K.NE. 0) REWIND K                                             OUTP027C
   3  IF (K) 3,4,3                                                      OUTP031C
      REWIND K                                                          OUTP032C
   4  RETURN                                                            OUTP033C
      END                                                               OUTP034C
```

```
      SUBROUTINE OUFT3                                              CLPT002C
C                                                                   CLPT001C
C     OUTPLT SUBROUTINE OUFT3                                       CLPT017C
C                                                                   CLPT003C
      DIMENSION B(50),OUTNO(50),ONAME1(50),ONAME2(50)               CLPT029C
      DIMENSION ONAME3(50)                                          CLPT007C
      COMMON C(3415)                                                CLPT010C
      INTEGER OUTCNT,PGCNT,CUTNO                                    CLPT011C
      EQUIVALENCE (C(2500),CUTNO(1))                                CLPT012C
      EQUIVALENCE (C(2550),ONAME1(1))                               CLPT013C
      EQUIVALENCE (C(2600),ONAME2(1))                               CLPT014C
      EQUIVALENCE (C(2650),ONAME3(1))                               CLPT015C
      EQUIVALENCE (C(2666),OUTCNT)                                  CLPT016C
      EQUIVALENCE (C(2667),ITCNT),(C(2668),PCNT),(C(2669),CPP)
      EQUIVALENCE (C(2661),NCOUT)
      EQUIVALENCE (C(2662),PGCNT)
      EQUIVALENCE (C(2671),TAPEND)
      EQUIVALENCE (C(2932),DER),(C(2671),TAPEND)
      EQUIVALENCE (C(2913),TAPE),(C(2298),YTP),(C(0306),ZTP)
      EQUIVALENCE (C(2670),XTP)
      EQUIVALENCE (C(2290),PUNCH)
      EQUIVALENCE (C(3400),PLET)
      EQUIVALENCE (C(3521),PSTI)
      EQUIVALENCE (C(0522),AXVECI)
      EQUIVALENCE (C(0544),AZVECI)
      EQUIVALENCE (C(0555),VXVECI)
      EQUIVALENCE (C(0577),VVVECI)
      EQUIVALENCE (C(0552),VXVECI)
      EQUIVALENCE (C(0547),YVECI)
      EQUIVALENCE (C(0549),ZVECI)
      IF(ITCNT .GT. 6) GO TO 7
   10 ITCNT = ITCNT + 1
      WRITE (6,6) (I,C(I),C(I+1),C(I+2),C(I+3),C(I+4),C(I+5),C(I+6),
     1 I=1,3415,8)
    6 FORMAT(1H1/(I5,2X,8E14.7))
      PGCNT = PGCNT + 1
    7 CONTINUE
      IF(T .LT. PCNT) RETURN
      IF(T - FCNT) 12,9,9
  100 RETURN
   12 PGCNT=PGCNT+CPP
      IF (PGCNT - NE. 1) GO TO 3
      IF (PGCNT - 1) 3,1,3
    1 WRITE(6,2) (ONAME1(I),ONAME2(I),ONAME3(I), I = 1, NOOUT)
```

```
    2 FORMAT (1H1,5X,4HTIME,5X,5(8X,3A4)//(23X,3A4,8X,3A4,8X,3A4,8X,    CLPT0450
     13A4,8X,3A4)/)                                                     CLPT0460
      PGCNT = 2*DTCNT + 4                                               CLPT0470
      IF (PGCNT .GE. 58) GO TO 1                                        CLPT0490
      IF (PGCNT - 58) 13,1,1                                            CLPT0510
   13 DO 4 I=1,NOUT                                                     CLPT0520
      J = OUTC(I)                                                       CLPT0530
    4 B(I) = TAPE(J)                                                    CLPT0540
      IF (K .NE. 0) WRITE (K) T,XTP,YTP,ZTP,TAPEND, (B(I),I=1,NCCUT)    CLPT0550
   14 IF (K) 15,14                                                      CLPT0560
   15 WRITE (6,5) T,XTP,YTP,ZTF,TAPEND,(B(I),I=1,NOOUT)                 CLPT0570
    5 FORMAT(F5.8,5F20.8/(17X,5F20.8))                                  CLPT0600
   22 FORMAT(F10.4,2F15.5)                                              CLPT0610
      IF(PUNCH-20,20,21                                                 CLPT0620
   21 WRITE(17,22) T,AXFCI,AYECI,AZECI,XECI,YECI,ZECI                   CLPT0630
   20 WRITE(17,22) T,VXECI,VYECI,VZECI,THET,PSI,PHI
      PGCNT = PGCNT + DTCNT + 4
      RETURN
      END

      SUBROUTINE STGF1                                                  S1GE0010
      RETURN                                                            STGE0020
      END                                                               STGE0030

      SUBROUTINE STGF2                                                  S1GE0010
      COMMON (3415)                                                     S1GE0020
      EQUIVALENCE (C(2904),KSTEP)                                       STGE0030
      EQUIVALENCE (C(2910),KCCNV)                                       STGE0040
      EQUIVALENCE (C(2672), LCONV)                                      STGE0050
      KCCNV=0                                                           STGE0060
      LCONV=0                                                           STGE0070
      KSTEP=1                                                           STGE0100
      RETURN                                                            STGE0120
      END

      SUBROUTINE STGF3                                                  S1GE0140
C THIS OPERATIONAL SUBROUTINE STAGES WHEN IMPACT IS MADE WITH THE       S1GE0010
C EARTH, WHEN FINAL TIME TF IS REACHED, OR WHEN ANOTHER PART OF THE     S1GE0020
```

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```
C     PROGRAM SETS LCONV = 2.  STAGING WILL OCCUR WHEN THE VEHICLE IS        STGE0030
C     WITHIN + CR.CCC1 SECOND OF TF, OR ACCORDING TO SOME CRITERION IN ANOTHER STGE0040
C     MODULE OR SUBROUTINE.  FOR EXAMPLE, IF STAGING IS DESIRED AT            STGE0060
C     COINCIDENCE BETWEEN A AND B, THE FOLLOWING FORTRAN STATEMENTS           STGE0070
C     SHOULD BE USED IN ONE OF THE SUBROUTINES OR MODULES --                  STGE0100
                                                                              STGE0110
      IF(ABS(A-B) .LE. 0.5) LCONV = 2                                         STGE0120
      IF(B .LT. 0.) LCONV = 1                                                 STGE0130
      DIMENSION STATNO(100),RMS(10)                                           STGE0270
      COMMON ...STATNO                                                        STGE0150
      INTEGER ...                                                             STGE0300
      EQUIVALENCE (C(932),T),(C(2913),DER)                                    STGE0160
      EQUIVALENCE (C(2668),PCNT) (C(0507),H)                                  STGE0170
      EQUIVALENCE (C(0550),TF),(C(2935),STEP)                                 STGE0210
      EQUIVALENCE (C(2904),KSTEP),(C(2671),TAPEAD)                            STGE0220
      EQUIVALENCE (C(2441),NOSTAT),(C(2200),STATNO(1)),(C(2430),RMS(1))       STGE0240
      EQUIVALENCE (C(2442),LCSTAT)                                            STGE0250
      EQUIVALENCE (C(2916),LCCNV)                                            STGE0310
      EQUIVALENCE (C(2672),LCONV)                                             STGE0320
      IF(T .LT. 1.0) GO TO 2                                                  STGE0330
      IF(B) 2,2,5                                                            STGE0340
    5 IF(A) 1,1,6                                                             STGE0350
    6 IF(TF .LE. 0.0001) GO TO 2                                              STGE0360
    7 IF(TF .LT. 0.0C1) 2,2,7                                                 STGE0370
      IF(TF) 8,8 GO TO 2                                                      STGE0400
    8 IF(TF .EQ. 2.) 9,2,9                                                    STGE0410
    9 IF(H .LT. 10.) GO TO 1                                                  STGE0420
      IF(H .GE. 10.) DER = -DER*0.5                                           STGE0430
      IF(DER .LT. 0.) 12,12                                                   STGE0440
   10 IF(DER-CER*0.5) 10,10,11                                                STGE0450
   11 RETURN                                                                  STGE0460
      IF(CER .GT. 0.) DER = -DER*0.5                                          STGE0470
   12 IF(DER-DER*0.5) 14,14,13                                                STGE0510
   13 IF(KCCNV-KCCNV + 1) GO TO 2                                             STGE0520
   14 IF(KCCNV .GE. 10) 15,2,2                                                STGE0530
   15 RETURN                                                                  STGE0540
      PCNT = 1.C                                                              STGE0550
      TAPEAD = 1.                                                             STGE0560
      CALL CLFT3                                                              STGE0600
      K = TAPE                                                                STGE0610
                                                                              STGE0620
                                                                              STGE0630
```

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```
C     IF (K .AE. 0) FND FILE K
      IF (K .AE. 0) REWIND K
   16 END FILE K
   17 REWIND K;16,17,16                                              TGF0640
C        IKSTEF = 2                                                  TGF0650
   18 IF (LCSTAT .EQ. NOSTAT) GO TO 4                                TGF0660
      IF (LCSTAT - NOSTAT) 18,4,18                                   TGF0670
      L = LCSTAT + 1                                                 TGF0700
      DO 3 I = L, NOSTAT                                             TGF0710
    3 RMS(I) = C(N)                                                  TGF0720
    4 RETURN                                                         TGF0730
      END                                                            TGF0740
C                                                                    TGF0750
                                                                     TGF0760
      SUBROUTINE CNTR1                                               TGF0770
C     RETURN                                                         TGF1000
C     END                                                            TGF1010

      SUBROUTINE CNTR2                                               CNTR0010
C     RETURN                                                         CNTR0020
C     END                                                            CNTR0030

      SUBROUTINE CNTR3                                               CNTR0010
C     RETURN                                                         CNTR0020
C     END                                                            CNTR0030

      SUBROUTINE RADM1                                               CNTR0010
CC    RETURN                                                         CNTR0020
      END                                                            CNTR0030

      SUBROUTINE RADM2                                               RADM0010
CCC   COMMON C(3415)                                                 RADM0020
C     EQUIVALENCE (C(2443), RNFLG)                                   RADM0030
      EQUIVALENCE (C(2446), ZN)
      EQUIVALENCE (C(2448), NCFNOM)
      EQUIVALENCE (C(2449), CELT)
      EQUIVALENCE (C(2450), RNCMNO)
      EQUIVALENCE (C(2913), CEF)
      DIMENSION RNCMNO(50)
      INTEGER RACMNO
```

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```
      IF (NGRADM) 2,2,3
3     RNFLG=C.C
      DELT=DER
      DO 1 I=1,NGRADM
      J=RADMNC(I)
      C(J+5)=2.718281828**(-DER*C(J+4))
      C(J+6)=C(J+3)*SQRT(1.0-C(J+5)*C(J+5))
      ZN=C(J+1)
      Y=INT(ZN,X)
1     N=C(J+7)=ZN
      CALL RFC(N,X)
      C(J+7)=C(J+1)=ZN
12    RETURN
      END


C
C
C
C
      SUBROUTINE RADM3
      COMMCN C(3415)
      EQUIVALENCE (C(2443), RNFLG)
      EQUIVALENCE (C(2444), RN)
      EQUIVALENCE (C(2446), ZA)
      EQUIVALENCE (C(2448), NORNDM)
      EQUIVALENCE (C(2449), DELT)
      EQUIVALENCE (C(2450), RADMNC)
      DIMENSIC RADMNQ(50)
      INTEGER RADMNO
10    IF (RNFLG.GE.1.0) GO TO 8
      IF (DER.GE.0.) GO TO 6
8     CO 9 I=1,NCRADM
      J=RADMNC(I)
9     X=(C(J+5)*C(J+8))/C(J+6)
      IF (RNFLG.GE.1.0) GO TO 5
      RNFLG=1.
      DELT=-DER
      DELT=DELT+DER
7     C(J+5)=2.718281828**(-DELT*C(J+4))
      C(J+6)=C(J+3)*X+C(J+5)*C(J+5)
      RETURN
5     IF (DELT.EG.DER) GO TO 4
2     CO 2 I=1,NCRADM
      J=RADMNC(I)
```

```
      C(J+5)=2.71828182B**(-DER*C(J+4))
    3 DELT=DER
    4 DO 1 I=1,NCRNDM
      J=RANAC(I)
      Y=C(J+1)
      ZN=INT(Y)
      N=INT(Y)
      CALL RFC(A,X)
      C(J+8)=C(J+7)
      C(J+7)=C(J+6)*X+C(J+5)*C(J+7)
      C(J+1)=ZN
   20 RETURN
      END
C
C
      SUBROUTINE AUXA1                                                  ALXA0010
      RETURN                                                           ALXA0020
      END                                                              ALXA0030
C
C
      SUBROUTINE AUXA2
      RETURN
      END
C
C
      SUBROUTINE AUXA3
      RETURN
      END
C
C
      SUBROUTINE AUXB1                                                  ALXB0010
      RETURN                                                           ALXB0020
      END                                                              ALXB0030
C
C
      SUBROUTINE AUXB2                                                  ALXB0010
      RETURN                                                           ALXB0020
      END                                                              ALXB0030
C
C
      SUBROUTINE AUXB3                                                  ALXB0010
      RETURN                                                           ALXB0020
      END                                                              ALXB0030
C
C
      SUBROUTINE AUXC1                                                  ALXC0010
      RETURN                                                           ALXC0020
```

```
C     END                                                          ALXC003C

C     SUBROUTINE ALXC2                                             ALXC001C
      RETURN                                                       ALXC002C
      END                                                          ALXC003C

C     SUBROUTINE AUXC3                                             ALXC0010
      RETURN                                                       ALXC002C
      END                                                          ALXC003C

C
C     SUBROUTINE RFG(M,X)
C
      COMMON C(3415)
      EQUIVALENCE (C(2446), ZN)
      Y=FLOAT(N)
      X=0.0
C     GENERATE UNIFORM RANDOM NO.(0 TO 1)
C     SUM FROM RAND NO(SIGMA=1,MEAN=0) FOR N=1
C     NORMAL DIST FOR LARGE N (12 OR GREATER)
      DO 1 I=1,N
      X=X+ZN-0.5*ZN
      RNO=SQRT.*ZN
    1 ZN=RNO-AINT(RNO)
      X=SQRT(12./Y)*X
      RETURN
      END

C
C     SUBROUTINE A11
C
C     AERODYNAMIC FORCES AND MOMENTS INITIALIZATION MODULE  A11
C     BODY AXES
C
      COMMON C(3415)
      EQUIVALENCE  (C(0208) , TSA )
      EQUIVALENCE  (C(0257) , CTS )
      EQUIVALENCE  (C(0258) , STS )
      CTS = COS(TSA)
      STS = SIN(TSA)
      RETURN
      END
C
```

```
      SUBROUTINE A1

C     AERODYNAMIC FORCES AND MOMENTS MODULE A1 - BODY AXES
C
      COMMON C(3415)
      EQUIVALENCE (C(110),S)
      EQUIVALENCE (C(111),CY)
      EQUIVALENCE (C(115),CZ)
      EQUIVALENCE (C(116),CBAR)
      EQUIVALENCE (C(189),CMG)
      EQUIVALENCE (C(190),CNF)
      EQUIVALENCE (C(211),CLP)
      EQUIVALENCE (C(223),CL)
      EQUIVALENCE (C(228),CM)
      EQUIVALENCE (C(229),CN)
      EQUIVALENCE (C(311),FXBA)
      EQUIVALENCE (C(132),FYBA)
      EQUIVALENCE (C(213),FZBA)
      EQUIVALENCE (C(214),CNBA)
      EQUIVALENCE (C(220),FBA)
      EQUIVALENCE (C(225),QBA)
      EQUIVALENCE (C(258),PBA)
      EQUIVALENCE (C(277),CCT)
      EQUIVALENCE (C(508),GCC)
      EQUIVALENCE (C(529),VAT)
C
      QDSC=CBAR*CBAR/(2.0*VAT)
      QDIM=CBAR/(2.0*VAT)
C     AERODYNAMIC MOMENTS (BODY AXES)
      CLBA=(CCL+CLP*DIM*PBA)
      CMBA=(CCM+CMQ*DIM*QBA)
      CNBA=(CCN+CNR*DIM*PBA)
C     AERODYNAMIC FORCES (BODY AXES)
      FXBA=CCX
      FYBA=CCY
      FZBA=CCZ
      RETURN
      END

      SUBROUTINE A2I
      RETURN
```

END

```
      SUBROUTINE A2

C  CAB  -- ZERO-LIFT BODY DRAG
C  CAC  -- DRAG DUE TO DEFLECTED CONTROL SURFACES
C  CAE+CAC
C  CZNB -- NORMAL FORCE DUE TO ANGLE OF ATTACK
C  CZNC -- NORMAL FORCE DUE TO FIN DEFLECTION
C  CYB  -- NORMAL FORCE DUE TO SIDESLIP
C  CYC  -- SIDE FORCE DUE TO FIN DEFLECTION
C  CZNR -- PITCH DAMPING MOMENT
C  CLP  -- ROLL DAMPING MOMENT
C  CPBC -- PITCH MOMENT DUE TO ANGLE OF ATTACK
C  CCNBC-- CONTROL SURFACE PITCH MOMENT
C  CMF+C-- YAW MOMENT DUE TO SIDESLIP
C  CCNBC-- CONTROL SURFACE YAW MOMENT
C  CLB+C-- INDUCED ROLL MOMENT
C  CLC  -- CONTROL SURFACE ROLL MOMENT

      COMMON/APPLE/TM1(7),TM2(15),TM3(14),TM4(5),TETA1(7),TETA2(7),
     1TETA3(6),TXT1(2),TXT2(10),TXI3(15),TDELT(5),TT1(3),TH2(2),
     2TCZBC(7,2),TDCZP(14,7),TCYBC(7,10,6),TCNBC(7,10,6),TDCNF(14,7),
     3TCLB(15,2),TCDC(15,2),TCAD2(15),TCNCA(15),TCMD1(15,4),
     4TCNC2(15,4),TCCMD(15,6),TCCNCA(15),TPMD(14,3),TCMQ(15),TPQ(14,3),
     5TCLBC(15),TCLD(15),TCCMSP(3),TPLD(14,3),TCLP(15),TPP(14,3),TDCYSP(3),
     LTCCZSP(3),TCCMSP(3),TCCNSP(3),TH3(3),TFEJ(13),TTEJ(13)
      EQUIVALENCE (CC(0016),DP)
      EQUIVALENCE (CC(0020),CG)
      EQUIVALENCE (CC(0024),CR)
      EQUIVALENCE (CC(0113),CA)
      EQUIVALENCE (CC(0114),CY)
      EQUIVALENCE (CC(0115),XII)
      EQUIVALENCE (CC(0116),CZN)
      EQUIVALENCE (CC(0117),CEAF)
      EQUIVALENCE (CC(0118),ETA)
      EQUIVALENCE (CC(0119),CNG)
      EQUIVALENCE (CC(0120),CAR)
      EQUIVALENCE (CC(0120),CLP)
```

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```
      EQUIVALENCE  (C(121),CN)
      EQUIVALENCE  (C(122),CLQ)
      EQUIVALENCE  (C(123),CLGR)
      EQUIVALENCE  (C(130),ALF)
      EQUIVALENCE  (C(133),BET)
      EQUIVALENCE  (C(134),CELLR)
      EQUIVALENCE  (C(150),DELP)
      EQUIVALENCE  (C(507),LBA)
      EQUIVALENCE  (C(511),VBAA)
      EQUIVALENCE  (C(518),SASA)
      EQUIVALENCE  (C(519),ESA)
      EQUIVALENCE  (C(525),VAT)
      EQUIVALENCE  (C(932),TT3)
      EQUIVALENCE  (C(935),TT4)
      EQUIVALENCE  (C(936),RDLL)
      EQUIVALENCE  (C(1696),RDUR)
      EQUIVALENCE  (C(1704),RDLR)
      EQUIVALENCE  (C(1708),FLGSEP)
      EQUIVALENCE  (C(1109),ZTP)
      EQUIVALENCE  (C(523),PHI)
      RAD=57.2957795
      ALF=ASA*RAD
      BET=ESA*RAD
      CDUR=RDUR*RAD
      CDLL=RDLL*RAD
      CDLR=RDLR*RAD
      DELG=RFLG*RAD
      CELF=CFR*RAD
      ADUR=AE*(CDUR)
      ADLL=AE*(CDLL)
      ADLR=AE*(CDLR)
      COSETA=VFAC*(EA/VAT)
      IF (COSETA.GE.1.0) COSETA=1.0
      ETA=EARCCS(COSETA)
      ETA=ETA*RAD
```

```
      VN=SQRT(VEA**2+WBA**2)
      IF(VN.LT.C.00001) GC TC 10
      XIR=ATAN2(VBA,WBA)
      GO TC 20
   10 XIR=C.C
   20 XII=XIR*RAD
      IF(XI1.LT.C.C) XI1=-XI
      XI2=XII
      IF(XII.GE.90.) XI2=180.-XI1
C     TABLE LCCK-LP,ALL PHASES
      CCZP=0.0
      PMC=1.0
      FNC=1.0
      PLC=1.0
      PQ=1..0
      PR=1..0
      PP=1..0
      CCASEP=CC
      CCLSEP=CC
      CCZSEP=CC
      CCASP=CC
      CCYSP=CC
C     MCMENT CCFFICIENTS
C     PITCHING MCMENT
      CMBC=THREDL(AM,XI2,FTA,TM1,TX13,TETA1,TCMBC,7,5,7)
      CCMUL=CCLI(AM,TM2,TCCMD,15)
      CCMUR=-CCMUL
      CCMLR=-CCMUL
      CCMULA=CCLI(AM,TM2,TCCMDA,15)
      CCMURA=-CCMULA
      CCMLRA=CCMULA
      CMG=CCLI(AM,TM2,TCMG,15)
C     YAWING MCMENT
      CNBC=THREDL(AM,XI2,FTA,TM1,TXI2,TETA3,TCNBC,7,10,6)
      IF(XII.GT.90.) CNBC=-CNBC
      IF(XI.LT.C.C) CNBC=-CNBC
      CCNUF=-CCPUL
      CCNLL=-CCNLL
      DCNULE=CCNLLA
```

```
      CCNURB=-CCMULA
      DCALLB=-CCMULA
      DCALRB=CCMULLA
C
C     ROLLING MOMENT
      CLBC=THRECL(AM,XI2,ETA,TM1,TXI2,TETA3,TCLBC,7,10,6)
      IF(XI1.LT.0.) CLBC=-CLBC
      IF(XI1.LT.90.) CLBC=-CLBC
      CLF=CDLI(AM,TM2,TCLD,15)
      CLLF=CDLI(AM,TM2,TCLF,15)
C
C     FORCE COEFFICIENTS
      CZBC=THRECL(AM,XI2,ETA,TM1,TXI2,TETA3,TCZBC,7,2,7)
      CYBC=THRECL(AM,XI2,ETA,TM1,TXI2,TETA3,TCYBC,7,10,6)
      IF(XI1.LT.0.) CYBC=-CYBC
      CAC2=CDLI(AM,TM2,TCAC2,15)
      IF(XI1.GT.0.) GO TO 100
CC    SEP AND BOOST PHASE
C     ZERO-LIFT DRAG
      CDB=STCLIA(TM2,TH2,TCDB,AM,H,15,2)
      IF(CDB.LT.0.08) CDB=.08
C     CONTROL SURFACE EFFECTIVENESS
      CMULC=STCLIA(TM2,TDELLT,TCMD1,AM,ADUL,15,4)
      IF(DLL.LT.0.0) CMULC=-CMULC
      CMURC=STCLIA(TM2,TDELLT,TCMD1,AM,ADUR,15,4)
      IF(DUR.LT.0.0) CMURC=-CMURC
      CMLLC=STCLIA(TM2,TDELLT,TCMD1,AM,ADLL,15,4)
      IF(DLL.LT.0.0) CMLLC=-CMLLC
      CMLRC=STCLIA(TM2,TDELLT,TCMD1,AM,ADLR,15,4)
      IF(DLR.LT.0.0) CMLRC=-CMLRC
C     FLUID EFFECTS
      IF(AM.GE.1.6) GO TO 200
      HOK=H/ICCC
      FM=2.12212E-06*HOK**3-5.20175-04*HOK**2+.044153*HOK-9.0995E-04
      DCCNP=STCLIA(TM3,TETA2,TDCNP,AM,ETA,14,7)
      IF(CCNP.LT.C.0) DCCNP=C.0
      DCCZP=STCLIA(TM3,TETA2,TDCCZP,AM,ETA,14,7)
      IF(CCZP.LT.0.0) DCZF=C.0
      DCCZF=CCZF+FM*FM
      PMC=STCLIA(TM3,THI,TFNC,AM,H,14,3)
      IF(FMC.GT.1.0) PMC=1.C
      FNC=FNC+FM
      PLC=STCLIA(TM3,THI,TFLC,AM,H,14,3)
      IF(FLC.GT.1.0) PLC=1.0
      FQ=STCLIA(TM3,THI,TFG,AM,H,14,3)
      IF(FQ.GT.1.C) PQ=1.C
      FR=PG
```

```fortran
      PP=STELIA(TM3,TH1,TEF,AM,H,14,3)
C     SEPARATION EFFECTS
      IF(FLGSEP.EO.0.) GO TC 200
      IF(PP.GT.1.0) PP=1.0
      IF(ZTP.GE.15.) GO TO 200
      IF(ZTP.GE.0.) GO TO 200
      FS2=(1.-ZTP/15.)*EXP(-ZTP/15.)
      DCCZNSPP=CCLLI(H,TH3,TECCZSP,3)
      DCZNSFP=FS2*DCZNSPP
      IF(ZTP.GE.4.0) GO TO 30
      FS1=(1.-ZTP/4.)*EXP(-ZTP/4.)
      DCCYSPP=CCLLI(H,TH3,TECCYSP,3)
      DCCNSPP=CCLLI(H,TH3,TECCNSP,3)
      DCCYSFP=FS1*DCCYSPP
   30 DCCNSFP=FS1*DCCNSPP
      CPHI=SIN(PHI)
      SPHI=CCS(PHI)
      DCCZNSEP=DCCZNSP*CPHI+DCYSP*SPHI
      DCCYSEP=DCCYSP*CPHI-DCZSP*SPHI
      DCCNSEP=DCCNSP*CPHI+DCNSP*SPHI
      DCCLSF=DCCLSP*CPHI-CCNSP*SPHI
C     TABLE LCCKUP FOR CRUISE PHASE
  100 CDC=STELIA(TM2,TCCC,AM,H,15,2)
C     CCNTRCL SURFACE EFFECTIVENESS
      CMULC=STELIA(TM4,TCDELT,TCMULO,AM,ADUL,5,4)
      IF(DULC.GT.O.) CMULC=-TCMULO
      CMURC=STELIA(TM4,TCDELT,TCMURO,AM,ADUR,5,4)
      IF(CURC.GT.O.) CMLRC=-TCMURO
      CMLLC=STELIA(TM4,TCDELT,TCMLLQ,AM,ADLL,5,4)
      IF(CLLC.GT.O.) CMLLC=-TCMLLQ
      CMLRC=STELIA(TM4,TCDELT,TCMLRO,AM,ADLR,5,4)
      IF(CLRC.GT.O.) CMLFC=-CMLRO
      CLLC=CLLR+.0017
C     END CF TABLE LCCK-UP
  200 CCNLLC=CALLLC
      CNURCC=-CALLRC
      CNLRC=CZBCC+CCZP
      CMEC=CCEC*CCSETA
      CABC=CCC*CCSETA
C     TRANSFORM FROM CROSS-FLCW TO BODY AXIS COMPCNENTS
```

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```fortran
      CXI=CCS(XIR)
      SXI=SIN(XIR)
      CAE=-CAEC*CXI-CZBC*SXI
      CYE=CYEC
      CZE=-CYBC*SXI+CZBC*CXI
      CLE=CLBC
      CMB=CMBC*CXI-CMBC*SXI
      CNB=CNBC
C
C     CONTROL SURFACE MOMENT AND FORCE COEFFICIENTS
C     CONTROL SURFACE CP IS 15.25 FT FROM NOSE
      F=(15.25-CG)/(15.25-CCR)
      CMUL=CMULC+DCMULA*ALF*CUL+DCMUL*ADUL
      CMUR=CMURC+DCMURA*ALF*CUR+DCMUR*ADUR
      CMLL=CMLLC+DCMLLA*ALF*CLL+DCMLL*ADLL
      CMLR=CMLRC+DCMLRA*ALF*CLR+DCMLR*ADLR
      CMC=(CMUL+CMUR+CMLL+CMLR)**F*PMD
      CNUL=CNULC+DCNULB*BET*CUL+DCNUL*ADUL
      CNUR=CNURC+DCNURB*BET*CUR+DCNUR*ADUR
      CNLL=CNLLC+DCNLLB*BET*DLL+DCNLL*ADLL
      CNLR=CNLRC+DCNLRB*BET*CLR+DCNLR*ADLR
      CNC=(CNUL+CNLL+CALR)**F*PND
      CLUL=CLULC*DUL
      CLLL=CLLLC*DLL
      CLLR=CLLRC*DLR
      CLCC=(CLUL+CLUR+CLLL+CLLR)*PLD
      CZC=-CBAR/(15.25-CG)
      CYC=-CAC2*(CUL**2+DUR**2+CLL**2+DLR**2+4.*1.3*(ALP*DELQ-BET*DELR))
C
C     TOTAL AERODYNAMIC FORCE COEFFICIENTS
      CY=CYE++CYC+CCYSEP
      CZ=CZB++CZC+CCZSEP
      CA=-I-CAC
      CZ=-I-CZ
C
C     TOTAL AERODYNAMIC MOMENT COEFFICIENTS
      CLF=CLE+CCLSEP
      CLL=CLF+CCLSEP
      CM=CMB+CZC+CZ9*(CG-CGR)/CBAR+CCMSEP
      CMG=CMG+RAC*PQ
      CN=CNB+CAC*CYB*(CG-CGR)/CBAR+CCNSEP
      CNR=CNR*RAC*PR
      RETURN
      END
```

```
SUBROUTINE A3I
COMMON C(3415)      FLG1
COMMON /FLAG/      FLG1      FF1)
EQUIVALENCE (C(9601), FF1)
EQUIVALENCE (C(9602), WEIG)
EQUIVALENCE (C(9603), IA)
EQUIVALENCE (C(9604), FLG2)
FF1=0.0
WEIG=0.0
IA=0
FLG1=0.0
FLG2=0.0
RETURN
END

SUBROUTINE A3

C     THIS IS THE MISSLE PROPULSION MODULE

C     TI=BOOST ENGINE IGNITION TIME
C     BT=BOOST ENGINE BURNOUT TIME(=T3)
C     BE=CRUISE ENGINE IGNITION TIME(=T4)

COMMON /FLAG/      FLG1      WEIGHT )
COMMON C(3415)    (C(0086) , S)
EQUIVALENCE (C(0110) , TI)
EQUIVALENCE (C(0932) , BT)
EQUIVALENCE (C(0935) , BE)
EQUIVALENCE (C(0936) , CG)
EQUIVALENCE (C(1360) , CLT)
EQUIVALENCE (C(1515) , CNT)
EQUIVALENCE (C(1152) , EPSTH)
EQUIVALENCE (C(1153) , PHITH)
EQUIVALENCE (C(2010) , A)
EQUIVALENCE (C(2020) , C)
EQUIVALENCE (C(2070) , TXBA)
EQUIVALENCE (C(0074) , TYBA)
EQUIVALENCE (C(0075) , TZBA)
EQUIVALENCE (C(0507) , T)
EQUIVALENCE (C(0520) , AMACH)
EQUIVALENCE (C(0117) , ETA)
```

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```fortran
      EQUIVALENCE (CC(06001), FF1)
      EQUIVALENCE (CC(06002), WEIG)
      EQUIVALENCE (CC(06003), TIA)
      EQUIVALENCE (CC(06004), FLG2)
      EQUIVALENCE (CC(06005), DIFFM)
      EQUIVALENCE (CC(06006), FLGRJ)
      EQUIVALENCE (CC(05008), GD)
      EQUIVALENCE (CC(2913), CER)
      DATA WFLEL/189./
C
   80 FORMAT(1H ,10X,'TOTAL ANGLE OF ATTACK EXCEEDED, ETA=',F8.2)
C
      IF (FLG1.GT.0.0) GO TO 10
      CDIFF=0.0
      FF=0.0
      TXBA=0.0
      TYEA=0.0
      TZBA=0.0
      IF(T.LT.T1) RETURN
      TIN=T-T1*.0254
      AIN=ETA
      IF(T.GE..EE) GO TO 1
C
      BCCST=T
      IF(T.GT.ET) GO TO 10
      CALL BCCST(TT,THRUS,FF)
      TXBA=THRUS*COS(EPSTH)
      TYBA=THRUS*SIN(EPSTH)
      TYBA=TXBA*SIN(PHIT)
      TZBA=TXBA*COS(PHIT)
      IB=0
      WEIGHT=WEIGHT-FF+FF1
      CG=CG+((FF-FF1)/405.54
      A=A-((FF-FF1)/256.25
      B=B-((FF-FF1)/1.881
      CC=B
      CLT=C
      CMT=TZEA*(15.525-CG)
      CNT=-TYEA*(15.525-CG)
      FF1=FF
      TW=T+DER
      IF(TW.LT.BT) GO TO 2
      IF(FLG2.GT.0.0) GO TO 2
      WEIG=WEIGHT-31.
      CG=CG-1.C
      FLG2=1.C
```

```
   10 GO TO 2
      CONTINUE
      IF(FLGRJ.GT.0.0) GO TO 21
C     CRUISE PHASE,RAMJET OFF
      IF(IB.GE.1)GO TO 11
      CALL ENGINE(HIN,AMACH,AIN,0.,TIN,1.0,0.,0.,CT,SMARG,-1,1)
   11 IB=1
      IF(AIN.GT.5.3) AIN=5.3
      CALL ENGINE(HIN,AMACH,AIN,0.,TIN,1.0,0.,0.,CT,SMARG,1,1)
      GO TO 4
C     SIMPLIFIED RAMJET MODEL
C     CRUISE PHASE,RAMJET OFF
   21 CALL RAMJET(HIN,AMACH,AIN,FF,1.0,CT)
      GO TO 4
    1 CONTINUE
      IF(FLGRJ.GT.0.0) GO TO 22
C     CRUISE PHASE,RAMJET ON
      IB=0
      IF(AIN.GT.10.0) GO TO 5
      FF=FF1
      IF(IA.GE.1) GO TO 3
      CALL ENGINE (HIN,AMACH,AIN,FF,TIN,0.0,0.0,0.0,CT,SMARG,-1,1)
      FF1=FF
    3 IA=1
      XIN=0.0
      IF(WEIG.GT.WFUEL) XIN=1.0
      CALL ENGINE (HIN,AMACH,AIN,FF,TIN,XIN,0.0,0.0,CT,SMARG,1,1)
      GO TO 4
C     SIMPLIFIED RAMJET MODEL
C     CRUISE PHASE,RAMJET ON
   22 XIN=0.0
      IF(AIN.GT.10.0) GO TO 5
      IF(WEIG.GT.WFUEL) XIN=1.0
      CALL RAMJET (HIN,AMACH,AIN,FF,XIN,CT)
      GO TO 4
    5 IF(FLG1.GT.0.0) GO TO 10
      WRITE(6,6) ETA
      FLG1=1.0
      GO TO 10
    4 TXBA=CT*GD*S
      TYBA=0.
      TZBA=C.
      CT=T-TT
      FF=FF/.45259237
      IF(FLGRJ.GT.0.0) GO TO 6
C     DIFFUSER (INLET) MARGIN IS NOT COMPUTED IN SIMPLIFIED RAMJET MODEL
      DIFFM=SMARG/100.
```

```
6     WEIG=WEIG+(ABS(FF+FF1))*DT/2.0
      IF(WEIG.GT.WFUEL) FLGI=1.0
      WEIGHT = WEIGHT - ABS(FF + FF1)*DT/2.
      TT=T
      FF1 = FF
      CG=CG-.0002645*ABS(FF+FF1)*DT/2.
      A=A-.0001746*ABS(FF+FF1)*DT/2.
      B=B-.0003492*ABS(FF+FF1)*DT/2.
      CC = B
2     RETURN
      END

C
C     SUBROUTINE A4I
C
C     ACTUATOR INITIALIZATION MODULE A4I
C
      COMMON C(3415)
      DIMENSION IPL(100),WFIN)
      EQUIVALENCE ((C(1735),WFIN)
      EQUIVALENCE ((C(3315),N)
      EQUIVALENCE ((C(3316),IPL(1))
      IF(FFIN.GT.C.0) GO TO 1C0
      GO TO 200
      IPL( 1)=1653
      IPL( 2)=1657
      IPL( 3)=1701
      IPL( 4)=1705
      IPL( 5)=1709
      IPL( 6)=1713
      IPL( 7)=1717
      IPL( 8)=1721
      N=N+8
200   RETURN
      END

C
C     SUBROUTINE A4
C
C     FIN ACTUATORS MODULE A4
C
      COMMON C(3415)
      EQUIVALENCE ((C(0016),CP)
      EQUIVALENCE ((C(0020),CG)
      EQUIVALENCE ((C(0024),DR)
      EQUIVALENCE ((C(1693),EULC)
```

```fortran
      EQUIVALENCE (C(1696),DUL)
      EQUIVALENCE (C(1697),DURC)
      EQUIVALENCE (C(1701),DLLC)
      EQUIVALENCE (C(1704),DLLC)
      EQUIVALENCE (C(1705),DLRC)
      EQUIVALENCE (C(1708),C1D)
      EQUIVALENCE (C(1709),C1)
      EQUIVALENCE (C(1712),C2C)
      EQUIVALENCE (C(1716),C3)
      EQUIVALENCE (C(1717),C4D)
      EQUIVALENCE (C(1721),WFIN)
      EQUIVALENCE (C(1724),DFIN)
      EQUIVALENCE (C(1735),DGC)
      EQUIVALENCE (C(1737),DRC)
      EQUIVALENCE (C(1738),DPC)
      EQUIVALENCE (C(1739),DMAX)
      EQUIVALENCE (C(1740),DULDEG)
      EQUIVALENCE (C(1734),DULDDG)
C     ACTUATOR INPUT MIXER
      DULC=DGC+DRC+DPC
      DURC=DGC+DRC+DPC
      DLLC=DGC-DRC+DPC
      DLRC=DGC-DRC+DPC
C     FIN ANGLE COMMAND LIMITERS
      IF(ABS(DULC).GT.DMAX) DULC=SIGN(DMAX,DULC)
      IF(ABS(DURC).GT.DMAX) DURC=SIGN(DMAX,DURC)
      IF(ABS(DLLC).GT.DMAX) DLLC=SIGN(DMAX,DLLC)
      IF(ABS(DLRC).GT.DMAX) DLRC=SIGN(DMAX,DLRC)
C     ACTUATOR DYNAMICS
      IF(VFIN.GT.0.0) GC TO 100
      GO TO
C     SECOND ORDER ACTUATORS
C     RATE AND DEFLECTION LIMITS
 9147
C     UPPER-LEFT FIN RESPONSE
100   D1C=WFIN*(DULC-DLL)-2.*DFIN*WFIN*C1
      IF(C1).GE.RTLIM) GC TO 110
      GO TO 120
110   PROD1=D1C*C1
      IF(PROD1.GE.0.0) D1C=0.0
120   DULD=CR1
C     UPPER-RT FIN RESPONSE
      C2C=WFIN*(DURC-DUR)-2.*DFIN*WFIN*D2
```

```
      IF (ABS(C2).GE.RTLIM)  GO TO 130
      GO TO 140
130   PROD2=C2D*C2
140   IF(PROD2.GE.0.0)  C2D=0.0
C           LOWER-LEFT  FIN RESPONSE
      C3D=-WFIN*WFIN*(DLLC-CLL)-2.*DFIN*WFIN*D3
      IF (ABS(C3).GE.RTLIM) GO TO 150
      GO TO 160
150   PROD3=C3D*C3
160   IF(PROD3.GE.0.0)  C3D=0.0
C           LOWER-RIGHT  FIN RESPONSE
      C4D=-WFIN*WFIN*(DLRC-CLR)-2.*DFIN*WFIN*D4
      IF (ABS(C4).GE.RTLIM) GO TO 170
      GO TO 180
170   PROD4=C4D*C4
180   IF(PROD4.GE.0.0)  C4D=0.0
      GO TO 20
C     ****  IDEAL ACTUATORS  ****
20    CUL=DULC
      CUR=DURC
      CLL=DLLC
      CLR=DLRC
C     FIN ANGLE LIMITERS
      IF(ABS(CUL).GT.DMAX)   CUL=SIGN(DMAX,DUL)
      IF(ABS(DUR).GT.DMAX)   DUR=SIGN(DMAX,DUR)
      IF(ABS(CLL).GT.DMAX)   CLL=SIGN(DMAX,DLL)
      IF(ABS(CLR).GT.DMAX)   CLR=SIGN(DMAX,DLR)
C     PITCH,YAW,RGLL CHANNEL INPUTS
220   DR=0.25*(-CUL-CUR-DLR+CLL)
      CP=0.25*(-CUL+DUR-DLR-CLL)
      CULCEG=CLL*57.29578
      CULCEG=CLLC*57.29578
      RETURN
      END
C
C     SUBROUTINE A5I
      RETURN
      END
C
C     SUBROUTINE A5
      RETURN
      END
```

```
      SUBROUTINE C1I
C
C   INITIALIZATION MODULE FOR LVRJ AUTOPILOT
C
      COMMON C(3415)
      EQUIVALENCE (C(3315),N)
      DIMENSION IPL(100)
      IPL(N+1)=1689
      IPL(N+2)=1725
      IPL(N+3)=1729
      N=N+4
      RETURN
      END


      SUBROUTINE C1
C
C   SUBROUTINE C1-LVRJ
C   THIS AUTOPILOT MODULE IS FOR STV G
C
      COMMON C(3415)
      EQUIVALENCE (C(0581),CYAP)
      EQUIVALENCE (C(0515),PSF)
      EQUIVALENCE (C(0520),AMACH)
      EQUIVALENCE (C(0415),C)
      EQUIVALENCE (C(0507),T)
      EQUIVALENCE (C(0932),T1)
      EQUIVALENCE (C(0935),T3)
      EQUIVALENCE (C(1636),ANZC)
      EQUIVALENCE (C(1640),ANYC)
      EQUIVALENCE (C(1644),ANZM)
      EQUIVALENCE (C(1648),AYM)
      EQUIVALENCE (C(1652),GM)
      EQUIVALENCE (C(1656),RM)
      EQUIVALENCE (C(0980),PM)
      EQUIVALENCE (C(1677),CPCID)
      EQUIVALENCE (C(1680),CFCI)
      EQUIVALENCE (C(1689),PI)
      EQUIVALENCE (C(1692),ZIC)
      EQUIVALENCE (C(1725),ZI)
      EQUIVALENCE (C(1728),Z1)
```

```
      EQUIVALENCE (CC(1729),Y1D)
      EQUIVALENCE (CC(1732),Y1R)
      EQUIVALENCE (CC(1737),CRC)
      EQUIVALENCE (CC(1738),CPC)
      EQUIVALENCE (CC(1739),CMAX)
      EQUIVALENCE (CC(1740),AKGY)
      EQUIVALENCE (CC(1165),AKGY)
      EQUIVALENCE (CC(1166),AKRF)
      EQUIVALENCE (CC(1167),AKFY)
      EQUIVALENCE (CC(1168),AKF)
      EQUIVALENCE (CC(1169),AKF)
      AKGI1=7.*C
      AKFI1=10.*C
      AKPI1=5.*C
      AKGI2=...C
      AKRI2=...C
      QCS=(2.*45/57.2957795
      CCE=1.*45/57.2957795
      IF(DYNP.GT.22.5) GO TO 3
      AKNY=.1
      AKNZ=.1
      IF(DYNP.GT.4.0) GO TO 4
      AKF=.8
      AKG=10.
      GO TO 8
    3 AKNY=.183502-.0157309S2*DYNP+3.183974E-04*DYNP**2-2.761728E-06*
     1 DYNP**4
      IF(DYNF.GT.45.)CC=27.
      AKNZ=.4514-.0027235*DYNP+6.307143E-04*DYNP**2-5.0E-06*DYNP**3
      IF(DYNF.GT.35.)CC=37.
      AKF=1.CE7-.1294302*DYNP+.007295*DYNP**2-1.93556E-04*DYNP**3
     1 +.E-06*DYNP**4
      AKG=1.790987-.08196419*DYNP+.0025119*DYNP**2-3.99521E-05*DYNP**3
      AKG=2.E2657-.302156*DYNP+.0177683*DYNP**2-4.99414E-04*DYNP**3
     1 +5.E-06*DYNP**4
      GO TO 8
    5 AKNZ=.CE225-.001225*DYNP
    6 AKF=.174143-.0028541E*DYNP+1.47619E-05*DYNP**2
      AKG=1.556357-.066502*DYNP+.0011233*DYNP**2-6.66666E-06*DYNP**3
      AKG=.4CE367*DYNP
    8 IF(AMACH.GT.2.0) GO TO 1
C     SEPARATION AND BOOST AUTCPILOT
      CC=GCS
      IF(T.GE.T1) QC=QCE
      S1=1.0
```

```
      S2=0.0
      AKGI=AKGI1
      AKRI=AKRI1
      AKPI=AKPI1
      GO TO 16
C     CRUISE ALTC FILCT
1     CONTINUE
      S1=0.0
      S2=1.0
      AKGI=AKGI2
      AKRI=AKRI2
      AKPI=AKPI2
16    CONTINUE
C     PITCH AND YAW CHANNELS
      GI=AKG*(GN-S1*QC)
      RI=AKR*(RN-S2*QC)
      ANYN=-ANZ/C
      ANZN=ANZC-ANZM
      ANY=AKNY-ANYN
C     POS DGC AND DRC COMMAND NEG TURNING MOMENTS
      CGC1=CGCC1
      Z1C=CG1-S2*AKNZ*ANZ     Z1D=0.0
      IF(ABS(CGC).GE.DMAX)    DGC=SIGN(DMAX,CGC)
      CGC=CGCC1+AKGI*Z1
      IF(ABS(CGC).GF.DMAX)    DGC=SIGN(DMAX,DMAX)
      CRC1=RI-S2*AKNY*ANY     Y1D=0.0
      Y1C=CRC1
      IF(ABS(CRC).GE.DMAX)    DRC=SIGN(DMAX,DRC)
      CRC=CRCC1+AKRI*Y1
      IF(ABS(CRC).GF.DMAX)    DRC=SIGN(DMAX,DRC)
2     CONTINUE
C     ROLL CHANNEL
      PIC=AKPI*FN
C     LAG COMPENSATOR
      CMG1=..C1
      CMG2=-.C1
      CPCC=-AKF*(FN+P1)*CMG2/CMG1
      CPCIC=(CMG1+CMG2)*CPCC-CMG2*DPCI
      DPC=CPCI+DFCC           DPC=SIGN(DMAX,DPC)
      IF(ABS(DPC).GF.DMAX)    DPC=SIGN(DMAX,DPC)
      RETURN
      END
C
C
C
C     SUBROUTINE C2I
```

```
      DIMENSION IPL(100)
      COMMON C(3415),C(0507),H
      EQUIVALENCE (C(3315),N)
      EQUIVALENCE (C(3316),IPL(1))
      IPL(N+1)=I
      IPL(N+2)=H
      N=N+2
      HNCW=H
      RETURN
      END


      SUBROUTINE C2

C     GUIDANCE COMMAND MODULE

      COMMON C(3415)
      EQUIVALENCE (C(0256),A33)
      EQUIVALENCE (C(0286),VXTP)
      EQUIVALENCE (C(0294),VZTP)
      EQUIVALENCE (C(0377),OMGZC)
      EQUIVALENCE (C(0387),OMGZC)
      EQUIVALENCE (C(0340),FLGT)
      EQUIVALENCE (C(0341),XMA)
      EQUIVALENCE (C(0520),YMA)
      EQUIVALENCE (C(0501),AMACH)
      EQUIVALENCE (C(0507),TCC)
      EQUIVALENCE (C(0507),TREF)
      EQUIVALENCE (C(0508),HD)
      EQUIVALENCE (C(0517),PSF)
      EQUIVALENCE (C(0527),GAMMAV)
      EQUIVALENCE (C(0531),VT)
      EQUIVALENCE (C(0581),CYNP)
      EQUIVALENCE (C(0593),AKG)
      EQUIVALENCE (C(0937),TT)
      EQUIVALENCE (C(0942),TCC)
      EQUIVALENCE (C(0944),TLC)
      EQUIVALENCE (C(0945),TFC)
```

```
      EQUIVALENCE (CC(1633),ANZCD)
      EQUIVALENCE (CC(1636),ANZC)
      EQUIVALENCE (CC(1637),ANYCD)
      EQUIVALENCE (CC(1640),ANYC)
      EQUIVALENCE (CC(1750),WFI)
      DATA RCC/144.4500./
C     ZERO MODE CONTROL SWITCHES
      S4=0...
      S5=0...
      S6=0...
      S8=0...
      IF(T.GE.T3) GO TO 1
C     SEPARATION...BOOST PHASE
      IF(AMACH.GE.2.0) GO TO 1
C     ZERO TRAJECTORY
    1 IF(T.GE.16C) GO TO 2
      GO TO 100
C     LEVEL FLIGHT
    2 IF(T.GE.TDC) GO TO 5
      S4=1.00
      GO TO 100
C     DIVE CLIMB
    5 IF(T.GE.TLC) GO TO 4
      HDCI=HDC
    7 S4=1...
      S5=1...
      S8=1...
      GO TO 100
C     AUTOMATIC LETDOWN TO HREF
    4 HORIZ=SQRT(XMA**2+YMA**2)
      D1=1.575*VH+RCCN-HORIZ
      IF(D1.GE.C.C) GO TO 6
      S4=1.00
      S5=1...0
      S6=1...0
      GO TO 100
C     TERMINAL DIVE
    6 W3=(ZMA*VYTP-XMA*VZTP)/(XMA*VXTP+ZMA*VZTP)
      ANZCI=-2.*2900.**W3/32.172+A33
      IF(FLC1.GT.0.0) GO TO 8
      GO TO 100
C     TERMINAL HOMING
    8 ANZCI=AKC*VT*OMGYC/32.174
  100 CONTINUE
```

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```
C      ***** VERTICAL CHANNEL *****
       HERR LIMITER=CG*(T-TREF)
       HERR1=CG*(T-TREF)
       HERRN2=CC5*HERR1
       IF(ABS(HERR1).GT.800.) HERR2=SIGN(400.,HERR1)
       ANZC1=.0333*(S8*HDC1-S4*(HD+HERR2))+S5*A33
C  NZ LIMITER
       IF(ANZC1) 108,107,108
108    AZMAX=.35*(DYNP-5.714)
       IF(DYNP.LE.30.0) AZMAX=.5*DYNP/30.
       AZMAX=AMIN1(AZMAX,12.0)
       IF(ABS(ANZC1).GE.AZMAX) ANZC1=SIGN(AZMAX,ANZC1)
107    CONTINUE
C      ***** LATERAL CHANNEL *****
       ANYC1=FLT-T5) GO TO 210
       IF(FLOAT.GT.0.0) GO TO 200
C  CROSS-FRODUCT MIDCOURSE GUIDANCE
       CPROD=(YMA*VXTP-XMA*VYTP)/(XMA*VXTP+YMA*VYTP)
       ANYC1=2600.*CPROD/32.172
       GO TO 207
C  TERMINAL HOMING
200    ANYC1=AKG*VT*OMGZC/32.172
C  NY LIMITER
201    IF(ANYC1) 208,207,208
208    AYMAX=.C*(DYNP-11.25)/22.5
       IF(DYNP.LE.22.5) AYMAX=4.0*DYNP/22.5
       AYMAX=AMIN1(AYMAX,12.0)
       IF(ABS(ANYC1).GT.AYMAX) ANYC1=SIGN(AYMAX,ANYC1)
207    CONTINUE
C      ***** ELLIPTICAL LIMITING *****
       DENOM=SGRT((AZMAX*ANYC1)**2+(AYMAX*ANZC1)**2)
       IF(DENOM.LE.0.0) GO TO 210
       AZLIM=AZMAX*AYMAX*ANZC1/CENOM     ANZC1=AZLIM
       AYLIM=AZMAX*AYMAX*ANYC1/CENOM     ANYC1=AYLIM
       IF(ABS(ANZC1).GE.ABS(AZLIM)) ANZC1=AZLIM
       IF(ABS(ANYC1).GE.ABS(AYLIM)) ANYC1=AYLIM
C      LATERAL COMMAND FILTER
210    ANYCC=KF1*(ANYC1-ANYC)
C      VERTICAL COMMAND FILTER
       ANZCC=KF1*(ANZC1-ANZC)
       RETURN
       END
C
CC     SUBROUTINE C3I
       RETURN
       END
```

```
C
      SUBROUTINE C3
      RETURN
      END
C
      SUBROUTINE C4I
      RETURN
      END
C
      SUBROUTINE C4
      RETURN
      END
C
      SUBROUTINE C5I
      RETURN
      END
C
      SUBROUTINE C5
      RETURN
      END
C
      SUBROUTINE C6I
      RETURN
      END
C
      SUBROUTINE C6
      RETURN
      END
C
      SUBROUTINE C7I
      RETURN
      END
C
      SUBROUTINE C7
      RETURN
      END
C
      SUBROUTINE C8I
```

```
      RETURN
      END
C
      SUBROUTINE C8
      RETURN
      END
C
      SUBROUTINE C9I
      RETURN
      END
C
      SUBROUTINE C9
      RETURN
      END
C
      SUBROUTINE C10I
      RETURN
      END
C
      SUBROUTINE C10
      RETURN
      END
C
      SUBROUTINE C11
C
C   TRANSLATIONAL DYNAMICS INITIALIZATION MODULE D1AB      C11A003C
C   FOR USE WITH MODULE C1A OR D1B                         C11A001C
C                                                          C11A002D
      DIMENSION IPL (100)                                  C11A007C
      COMMON C(3415)                                       C11A004Q
      EQUIVALENCE (C(3315),A)                              C11A005C
      EQUIVALENCE (C(3316),IPL(1))                         C11A0100
      IPL(1) = 283                                         C11A011C
      IPL(2) = 291                                         C11A012C
      IPL(3) = 299                                         C11A013C
      IPL(4) = 287                                         C11A014C
      IPL(5) = 295                                         C11A015C
      IPL(6) = 303                                         C11A016C
      RETURN                                               C11A017C
      END                                                  C11A020C
```

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```
SUBROUTINE C1

TRANSLATIONAL DYNAMICS MODULE D1B - BODY AXES

      COMMON C(3415)
      EQUIVALENCE (C(0073),TXBA)
      EQUIVALENCE (C(0074),TYBA)
      EQUIVALENCE (C(0075),TZBA)
      EQUIVALENCE (C(0086),FE...)
      EQUIVALENCE (C(0128),FXBA)
      EQUIVALENCE (C(0129),FYBA)
      EQUIVALENCE (C(0130),FZBA)
      EQUIVALENCE (C(0224),A11)
      EQUIVALENCE (C(0228),A12)
      EQUIVALENCE (C(0232),A13)
      EQUIVALENCE (C(0236),A21)
      EQUIVALENCE (C(0240),A22)
      EQUIVALENCE (C(0244),A23)
      EQUIVALENCE (C(0248),A31)
      EQUIVALENCE (C(0252),A32)
      EQUIVALENCE (C(0256),A33)
      EQUIVALENCE (C(0283),AG)
      EQUIVALENCE (C(0286),VXDTP)
      EQUIVALENCE (C(0287),VXXTP)
      EQUIVALENCE (C(0291),VYDTP)
      EQUIVALENCE (C(0294),VYYTP)
      EQUIVALENCE (C(0295),VZDTP)
      EQUIVALENCE (C(0298),VZZTP)
      EQUIVALENCE (C(0302),ZTP)
      EQUIVALENCE (C(0306),CCX)
      EQUIVALENCE (C(0411),CCY)
      EQUIVALENCE (C(0412),CCZ)
      EQUIVALENCE (C(0710),TAXBA)
      EQUIVALENCE (C(0712),TAYBA)
      EQUIVALENCE (C(0713),TAZBA)
      EQUIVALENCE (C(0714),TAX))
      EQUIVALENCE (C(0714),TAY))
      EQUIVALENCE (C(0715),TAZ))

      AGWE = AG/W
```

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C     TOTAL ACCELERATION DUE TO AERODYNAMIC FORCES AND THRUST FORCES
      TAXBA = AGXE*(FXBA + TXBA)
      TAYBA = AGYE*(FYBA + TYBA)
C     TAZBA = AGZE*(FZBA+TZBA+FEJ)
      RESOLVE FROM BODY AXES TO TANGENT PLANE
      TAX = A11*TAXBA + A21*TAYBA + A31*TAZBA
      TAY = A12*TAXBA + A22*TAYBA + A32*TAZBA
      TAZ = A13*TAXBA + A23*TAYBA + A33*TAZBA
C     INTEGRATE ACCELERATIONS DUE TO AERODYNAMICS, THRUST, GRAVITY,
      AND COEFFICLIS
CC    VXDTP = TAX + GCX
      VYDTP = TAY + GCY
      VZDTP = TAZ + GCZ
C     INTEGRATE VELOCITY
      XDTP = VXTP
      YDTP = VYTP
      ZDTP = VZTP
      RETURN
      END

      SUBROUTINE C2I
CCC   ROTATIONAL DYNAMICS INITIALIZATION MODULE D2IEUL
CCCC  FOR USE WITH MODULE C2F OR D2SA
      COMMON C(3415)
      EQUIVALENCE (C(224) , A11 )
      EQUIVALENCE (C(228) , A12 )
      EQUIVALENCE (C(232) , A21 )
      EQUIVALENCE (C(236) , A22 )
      EQUIVALENCE (C(240) , A23 )
      EQUIVALENCE (C(244) , A31 )
      EQUIVALENCE (C(248) , A32 )
      EQUIVALENCE (C(252) , A33 )
      EQUIVALENCE (C(256) , ROLLO )
      EQUIVALENCE (C(2901) , PITCHO )
      EQUIVALENCE (C(2902) , YAWN )
      EQUIVALENCE (C(2903) , )
      EQUIVALENCE (C(3315) , IPL )
      EQUIVALENCE (C(100) , IPL )
      DIR=SIN(ROLLO)
      SP=SIN(PITCHO)
      CT=COS(PITCHO)
      EQUIVALENCE (C(3316) , IPL(1))
      SS=SIN(YAWO)
      CS=COS(YAWO)
```

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```
CP = CCS(RCLLO)
A11 = CCT
A12 = -CT
A21 = -CT *CP + CS*ST*SP
A22 = CCV +SS*ST*SP
A23 = -CT *CF + SS*SP
A31 = CCVST*CF + SS*SP
A32 = CCVST*CF *CP - CS*SP
A33 = -CT *CF
IPL = 2CS
IPL =          213
IPL =          217
IPL =          221
IPL =          225
IPL =          229
IPL =          233
IPL =          237
IPL =          241
IPL =          245
IPL =          249
IPL =          253
RETURN
END

SUBROUTINE C2
ROTATIONAL DYNAMICS MODULE D2PA- PRINCIPAL AXES
COMMON C(3415)
COMMON/APFLE/TM1(7),TM2(15),TM3(14),TM4(5),TETA1(7),TETA2(7),
1TXI1(2),TXI2(10),TXI3(5),TDELT(4),TH1(3),TH2(2),TH3(3),
2TCZBC(6),TDCZP(14,7),TCYBC(7,10,6),TCNBC(7,5,7),TDCMF(14,7),
3TCCBC(15,2),TCAD2(15),TCNBC(7,10,6),TCMDI(15,4),
4TCLMD(15,2),TCCMD(15),TPMD(14,3),TCMQ(15),TPQ(14,3),
5TCLBD(5),TCLD(16),TPLD(14,3),TCLP(15),TPP(14,3),TDCYSP(3),
LTDCZSP(3),TCCMSP(3),TCCNSP(3),FLGSEP)
EQUIVALENCE (C(0109),FEJ        )
EQUIVALENCE (C(0112),CLBA       )
EQUIVALENCE (C(0132),CNBA       )
EQUIVALENCE (C(0136),CG)
EQUIVALENCE (C(0150),CLT        )
EQUIVALENCE (C(0151),CMT        )
```

```
      EQUIVALENCE ( . . , . . )            CNT
      EQUIVALENCE ( . . , . . )          E PDBA
      EQUIVALENCE ( . . , . . )          C PBA
      EQUIVALENCE ( . . , . . )          CDBA
      EQUIVALENCE ( . . , . . )          GDBA
      EQUIVALENCE ( . . , . . )          RDBA
      EQUIVALENCE ( . . , . . )          FBA
      EQUIVALENCE ( . . , . . )          AD11
      EQUIVALENCE ( . . , . . )          AD12
      EQUIVALENCE ( . . , . . )          AD13
      EQUIVALENCE ( . . , . . )          A21
      EQUIVALENCE ( . . , . . )          AD22
      EQUIVALENCE ( . . , . . )          AD23
      EQUIVALENCE ( . . , . . )          A31
      EQUIVALENCE ( . . , . . )          AD32
      EQUIVALENCE ( . . , . . )          A32
      EQUIVALENCE ( . . , . . )          AC33
      EQUIVALENCE ( . . , . . )          AC31
      EQUIVALENCE ( . . , . . )          T1

      X=(T1 .LE. C .C.)   FLGSEP=0.0
10    IYW=(FLGSEP .LE. 0.) GO TO 10
      IF (FLGSEP .LE. 0.) GO TO 10

C     FEJ=CDLI(...AMIC,THRUST,AND EJECTION MOMENTS)
      ACCLEA=CLEA+...                    DYNAMIC...
      TMEA=0
      TNEA=CNEA+CONT
C     INTEGRATE BODY ANGULAR RATES
      PDBA = +(B-G)*GBA*RBA)/A
      GDBA = (TLBA + (G-I)*REA*PBA)/B
      RDBA = (TNBA + (A-B)*PBA*QBA)/G
C     INTEGRATE ATTITUDE DIRECTION COSINES
      AD11=A21*QEA-A31*QEA
```

```
      AD22=A32*PBA-A12*RBA
      AD21=A31**FBA-A11**RBA
      AD13=A22**RBA-A33**QBA
      AD12=A22**FBA-A32**PBA
      AD32=A11**GBA-A23**PBA
      AD31=A11**GEA-A21**PBA
      AD23=A12**PBA-A13**RBA
      RETURN
      END

      SUBROUTINE C3I
      RETURN
      END

      SUBROUTINE D3
      RETURN
      END

      SUBROUTINE C4I
      RETURN
      END

      SUBROUTINE C4
      RETURN
      END

      SUBROUTINE C5I
      RETURN
      END

      SUBROUTINE C5
      RETURN
      END

      SUBROUTINE G1I
C     GRAVITATIONAL AND CORIOLIS ACCELERATION INITIALIZATION MODULE G1IC
      COMMON C(3415)
```

```
      EQUIVALENCE (C(0402))  ZS
      EQUIVALENCE (C(0405))  GM
      EQUIVALENCE (C(0407))  ER
      EQUIVALENCE (C(0409))  ALPO
      EQUIVALENCE (C(0410))  CLAMO
      EQUIVALENCE (C(0414))  OMEGX
      EQUIVALENCE (C(0415))  OMEGY
      EQUIVALENCE (C(0502))  OMEGZ
      EQUIVALENCE           GO
      EQUIVALENCE           RE
      ZS = RE + ZS
      GM = GER * ZS
      RT = RE + RT*COS(CLAMO)
      CMEGZ = RT = -RT*SIN(CLAMO)
      OMEGY = -RT*SIN(ALPO)
      OMEGX = RT*COS(ALPO)
      RETURN
      END


      SUBROUTINE G1
C
C     GRAVITATIONAL AND CORIOLIS ACCELERATION MODULE GIC
C
      COMMON (3415)
      EQUIVALENCE (C(0288))  VXTP
      EQUIVALENCE (C(0294))  VYTP
      EQUIVALENCE (C(0302))  VZTP
      EQUIVALENCE (C(0298))  XTP
      EQUIVALENCE (C(0301))  YTP
      EQUIVALENCE (C(0402))  ZTP
      EQUIVALENCE (C(0403))  ZS
      EQUIVALENCE (C(0404), GM)  GZRO
      EQUIVALENCE (C(0408))  OMEGX
      EQUIVALENCE (C(0409))  OMEGY
      EQUIVALENCE (C(0411))  OMEGZ
      EQUIVALENCE (C(0412))  CCX
      EQUIVALENCE (C(0413))  CCY
      EQUIVALENCE (C(0414))  CCZ
      EQUIVALENCE (C(0415))  GO
      EQUIVALENCE (C(5002),HC), RE
```

```
      EQUIVALENCE (CC(0507),+ )
      EQUIVALENCE (CC(0507),+ )
      IF(GZRC .EQ. 1.0) GO TO 1
C     COMPUTE FLAT-EARTH GRAVITATIONAL FIELD
C     FLAT-EARTH GRAVITATIONAL ACCELERATION
      GCX= . . .
      GCY= . . .
      GCZ= . . . +HC
      HD= -VZTF
      HD= -VZTF
      RETURN
C
    1 R = SQRT(XTP*XTP + YTP*YTP + (ZTP-ZS)*(ZTP-ZS))
      HD=(XTF*VXTF+YTP*VYTF+(ZTP-ZS)*VZTP)/R
C     COMPUTE SPHERICAL GRAVITATIONAL FIELD
      R = RU/(R*R)
C     SPHERICAL GRAVITATIONAL ACCELERATION
      GMR = GM/(R*R*R)
      GCX = GMR*XTP
      GCY = GMR*YTP
      GCZ = GMR*(ZTP-ZS)
C     ADD CORIOLIS ACCELERATION
      GCX = GCX + OMEGZ*VYTP - OMEGY*VZTP
      GCY = GCY + OMEGX*VZTP - OMEGZ*VXTP
      GCZ = GCZ + OMEGY*VXTP - OMEGX*VYTP
      RETURN
      END
C
C
      SUBROUTINE G2I
      RETURN
      END
C
C
      SUBROUTINE G2
      RETURN
      END
C
C
C
      SUBROUTINE G3I
      COMMON (3415)
      EQUIVALENCE (CC(0208) , TSA )
      EQUIVALENCE (CC(0257) , CTS )
      EQUIVALENCE (CC(0306) , STS )
      EQUIVALENCE (CC(0414) , HC )
      EQUIVALENCE (CC(0507) , H )
```

```
EQUIVALENCE (C(0515), FSF)
EQUIVALENCE (C(0529), VAT)
EQUIVALENCE (C(0551), RHCH)
EQUIVALENCE (C(0561), VAT)
ALT=(ALT)/3.280839895
VEL=VAT/.280839895
CALL ATF(ALT,VEL,-1,P,T,SON,DEN,Q,G,1,2)
CTS = CS(TSA)
STS = SIN(TSA)
RETURN
END

SUBROUTINE G3
AIR DATA MODULE G3
COMMON (3415)
EQUIVALENCE (C(0224), A11)
EQUIVALENCE (C(0228), A12)
EQUIVALENCE (C(0236), A13)
EQUIVALENCE (C(0244), A21)
EQUIVALENCE (C(0248), A22)
EQUIVALENCE (C(0256), A23)
EQUIVALENCE (C(0257), A31)
EQUIVALENCE (C(0258), A32)
EQUIVALENCE (C(0289), A33)
EQUIVALENCE (C(0290), CTS)
EQUIVALENCE (C(0291), STS)
EQUIVALENCE (C(0451), AG)
EQUIVALENCE (C(0452), VXTP)
EQUIVALENCE (C(0456), VYTP)
EQUIVALENCE (C(0505), VZTP)
EQUIVALENCE (C(0506), TWXTP)
EQUIVALENCE (C(0507), TWYTP)
EQUIVALENCE (C(0509), TWZTP)
EQUIVALENCE (C(0510), VATX)
EQUIVALENCE (C(0511), VATY)
EQUIVALENCE (C(0512), VATZ)
EQUIVALENCE (C(0513), TGD)
EQUIVALENCE (C(0511), LBA)
EQUIVALENCE (C(0512), VBA)
EQUIVALENCE (C(0511), USA)
EQUIVALENCE (C(0511), VSA)
```

C C C   C C C

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      EQUIVALENCE (CC(0514) ,PSA )
      EQUIVALENCE (CC(0515) ,PSF )
      EQUIVALENCE (CC(0518) ,ESA )
      EQUIVALENCE (CC(0519) ,ANACH )
      EQUIVALENCE (CC(0520) ,AMACH )
      EQUIVALENCE (CC(0522) ,VAT )
      EQUIVALENCE (CC(0551) ,RTCH )
      EQUIVALENCE (CC(0561) ,VAH )
C     VELOCITY WITH RESPECT TO AIR MASS
      VATX = TWXTP
      VATY = TWYTP
      VATZ = TWZTP
      VATSQ = VATX*VATX + VATY*VATY + VATZ*VATZ
      VAT = SQRT(VATSQ)
      ALT = .28083989 5
      VEL = VAT
      CALL AIR (ALT,VEL,1,P,T,SON,DEN,Q,G,1,2)
      PSF = .434.7661*DEN
      RTCH = .0144*Q
      GD = .95*SON
      VAHCHG = VAT/VAH
C     ORTHOGONALIZE DIRECTION COSINES
      CAN = SQRT(A11**2+A12**2+A13**2)
      E11 = A11/CAN
      E12 = A12/CAN
      E13 = A13/CAN
      C2 = E12*A22+E13*A23
      CON = V21**2+V22**2+V23**2
      E21 = A21-C2*E11
      E22 = A22-C2*E12
      E23 = A23-C2*E13
      CAP = SQRT(V31**2+V32**2+V33**2)
      A31 = E12*A32+E13*A33
      A12
      A21
```

```
      A22=E22
      A31=E31
      A32=E32
      A33=E33
C     VELOCITY IN BODY AXES
      UBA=A11*VATX+A12*VATY+A13*VATZ
      VBA=A21*VATX+A22*VATY+A23*VATZ
      WBA=A31*VATX+A32*VATY+A33*VATZ
C     VELOCITY IN STABILITY AXES
      USA=CTS*UBA+STS*WBA
      VSA=VBA
      WSA=-STS*UBA+CTS*WBA
C     ANGLE OF ATTACK AND SIDESLIP
      ASA = ATAN(WSA/USA)
      BSA = ARSIN(VSA/SQRT(USA*USA + VSA*VSA + WSA*WSA))
      RETURN
      END
C
      SUBROUTINE G4I
      RETURN
      END
C
      SUBROUTINE G4
      RETURN
      END
CC
      SUBROUTINE G5I
CC
CCC   COORDINATE CONVERSION INITIALIZATION MODULE
CCC
      COMMON C(3415)
      EQUIVALENCE (C(0557),CTPHI11)
      EQUIVALENCE (C(0558),CTPHI12)
      EQUIVALENCE (C(0559),CTPHI13)
      EQUIVALENCE (C(0562),CTPHI21)
      EQUIVALENCE (C(0563),CTPHI22)
      EQUIVALENCE (C(0564),CTPHI23)
      EQUIVALENCE (C(0566),CTPHI31)
      EQUIVALENCE (C(0577),ALAT)
      EQUIVALENCE (C(0578),AZ)
      AZ = AZ*.01745329
```

TXY0126C
TXY0127C
TXY0128C

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```
      ALAT = ALAT*.01745329
      CTFI111 =-COS(AZ)*SIN(ALAT)
      CTPI112 = -SIN(ALAT)*SIN(AZ)
      CTFI113 = -COS(ALAT)
      CTFI121 = SIN(AZ)
      CTFI122 = COS(AZ)
      CTFI123 = 0.
      CTFI131 = -COS(ALAT)*COS(AZ)
      CTPI132 =-COS(ALAT)*SIN(AZ)
      CTFI133 = -SIN(ALAT)
      RETURN
      END

      SUBROUTINE G5
C     COORDINATE CONVERSION MODULE G5
      COMMON C(3415)
      EQUIVALENCE (C(0224),CTFB11)
      EQUIVALENCE (C(0228),CTFB12)
      EQUIVALENCE (C(0230),CTFB13)
      EQUIVALENCE (C(0236),CTFB21)
      EQUIVALENCE (C(0240),CTPB22)
      EQUIVALENCE (C(0244),CTFB23)
      EQUIVALENCE (C(0256),CTFB31)
      EQUIVALENCE (C(0557),CTFB32)
      EQUIVALENCE (C(0558),CTFB33)
      EQUIVALENCE (C(0560),CTFI111)
      EQUIVALENCE (C(0562),CTFI112)
      EQUIVALENCE (C(0564),CTFI113)
      EQUIVALENCE (C(0565),CTPI121)
      EQUIVALENCE (C(0567),CTFI122)
      EQUIVALENCE (C(0569),CTFI123)
      EQUIVALENCE (C(0571),CTFI131)
      EQUIVALENCE (C(0572),CTFI132)
      EQUIVALENCE (C(0574),CTFI133)
      EQUIVALENCE (C(0574),CEII11)
      EQUIVALENCE (C(0575),CEII12)
      EQUIVALENCE (C(0576),CEII13)
      EQUIVALENCE (C(0071C),CEII21)
      EQUIVALENCE (C(0071C),CEII22)
      EQUIVALENCE (C(0071C),CEII23)
      EQUIVALENCE (C(0071C),CEII31)
      EQUIVALENCE (C(0071C),CEII32)
      EQUIVALENCE (C(0071C),CEII33,TAXAA)
```

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      EQUIVALENCE (C00711,TAYAA))
      EQUIVALENCE (C00712,TAZAA))
      EQUIVALENCE (C00286,VXTP))
      EQUIVALENCE (C00264, VYTP))
      EQUIVALENCE (C00300,VZTP))
      EQUIVALENCE (C00290,ZTP))
      EQUIVALENCE (C00268,THET))
      EQUIVALENCE (C00521,AXECII))
      EQUIVALENCE (C00544,AXECII))
      EQUIVALENCE (C00555,AYECII))
      EQUIVALENCE (C00577,AZECII))
      EQUIVALENCE (C00522,VXECII))
      EQUIVALENCE (C00547,VYECII))
      EQUIVALENCE (C00540,VZECI))
      EQUIVALENCE (C00402,NS))
      EQUIVALENCE (C00523,PSI))
      EQUIVALENCE (C00524,PHI))
      EQUIVALENCE (C00526,BEAR))
      EQUIVALENCE (C00527,ELEV))
      EQUIVALENCE (C00531,SLANT))
      EQUIVALENCE (C00528,VGS))
      EQUIVALENCE (C00532,VH))
      EQUIVALENCE (C00532,GAMMAV))
      EQUIVALENCE (C00532,GAMMAH))
C
C MATRIX HEADING
      MATRIX HEADING = ATAN(CTPB,RCLL)
      PSIT=ATAN(CTPB12,CTPB11)
      THET = ARSIN(CTPB13)
      PHIR = ATAN2(CTPB23,CTFE33)
C FLIGHT PATH
      VH=SQRT(VXTP*VXTP + VYTP*VYTP)
      GAMMAH = ATAN(-VZTP,VXTP/VH)
      GAMMAV = ATAN2(VYTP,VXTP)
C RANGE AND TOTAL VELOCITY
C SLANT RANGE AND ELEVATION
      SLANT = SQRT(XTP*XTP + YTP*YTP + ZTP*ZTP)
      VGS = SQRT(VXTP*VXTP + VYTP*VYTP + VZTP*VZTP)
C BEARING
      IF(YTP)1,3,1
      BEAR=C.4
      GO TO C.2
  1   BEAR=ATAN2(YTF,XTP)
  2   CONTINUE
      IF(XTP.EQ.0.0 .AND. YTP.EQ.0.0) GO TO 50
```

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```fortran
      ELEV = ATAN (-ZTP/SQRT(XTP*XTP + YTP*YTP))
      GO TO 60
   50 ELEV=0.0
   60 CONTINUE
C
      CEI = CTPI*CETP
      CCBI111*CTPI11 + CTPI12*CTPB12 + CTPI13*CTPB13
      CCBI112*CTPI11 + CTPI12*CTPB22 + CTPI13*CTPB23
      CCBI121*CTPI21 + CTPI22*CTPB12 + CTPI23*CTPB13
      CCBI122*CTPI21 + CTPI22*CTPB22 + CTPI23*CTPB23
      CCBI131*CTPI31 + CTPI32*CTPB12 + CTPI33*CTPB13
      CCBI132*CTPI31 + CTPI32*CTPB22 + CTPI33*CTPB23
      CCBI133*CTPI31 + CTPI32*CTPB32 + CTPI33*CTPB33
C
C     DETERMINE ACCELERATION, VELOCITY AND POSITION IN ECI SYSTEM
C
      AXECI = CTPI11*TAXAA + CTPI12*TAYAA + CTPI13*TAZAA
      AYECI = CTPI21*TAXAA + CTPI22*TAYAA + CTPI23*TAZAA
      AZECI = CTPI31*TAXAA + CTPI32*TAYAA + CTPI33*TAZAA
      VXECI = CTPI11*VXTP + CTPI12*VYTP + CTPI13*VZTP
      VYECI = CTPI21*VXTP + CTPI22*VYTP + CTPI23*VZTP
      VZECI = CTPI31*VXTP + CTPI32*VYTP + CTPI33*VZTP
      XECI = CTPI11*XTP + CTPI12*YTP + CTPI13*(ZTP - ZS)
      YECI = CTPI21*XTP + CTPI22*YTP + CTPI23*(ZTP - ZS)
      ZECI = CTPI31*XTP + CTPI32*YTP + CTPI33*(ZTP - ZS)
      RETURN
      END
C
      SUBROUTINE G6I
      RETURN
      END
C
      SUBROUTINE G6
      RETURN
      END
C
      SUBROUTINE S1I
C
C     HOMING SEEKER INITIALIZATION MODULE   S1I
C
      COMMON C(3415)
      DIMENSION IFL(100), FLGT)
      EQUIVALENCE ((C(03117), FLGT)
      EQUIVALENCE ((C(03347), FLGTS)
      EQUIVALENCE ((C(33315), A)
      EQUIVALENCE ((C(33316), IPL(1))
```

```
IPL(A)=262
IPL(A+1)=2266
IPL(A+2)=2704
IPL(A+3)=2266
IPL(A+4)=4204
IPL(A+5)=4424
IPL(A+7)=4428
IPL(A+8)=4428
A=A+10
FLCTS=C.C
FLCTSR=C.0
RETURN
END

SUBROUTINE S1
HOMING SEEKER MODULE S1

COMMON /C(3415)/
EQUIVALENCE (C(187), CNCTS1)
EQUIVALENCE (C(197), CNCTS2)
EQUIVALENCE (C(212), P)
EQUIVALENCE (C(220), R)
EQUIVALENCE (C(262), CNZGYD)
EQUIVALENCE (C(265), CNZGYD)
EQUIVALENCE (C(269), CNZGZD)
EQUIVALENCE (C(270), CNZ)
EQUIVALENCE (C(273), THTSD)
EQUIVALENCE (C(274), PSISD)
EQUIVALENCE (C(277), PSISD)
EQUIVALENCE (C(279), CNZGYS)
EQUIVALENCE (C(286), ANGLT)
EQUIVALENCE (C(317), RS)
EQUIVALENCE (C(318), FLCT)
EQUIVALENCE (C(320), RMTT)
EQUIVALENCE (C(321), XYDTT)
EQUIVALENCE (C(322), CNZCCID)
EQUIVALENCE (C(325), CNZCCID)
EQUIVALENCE (C(326), CNZYCID)
EQUIVALENCE (C(329), CNZYCI)
```

      CCC   CCC

```fortran
      EQUIVALENCE (C(351), FLAGS)
      EQUIVALENCE (C(336), FLGGD)
      EQUIVALENCE (C(337), CNGYC)
      EQUIVALENCE (C(338), CNG2C)
      EQUIVALENCE (C(342), RXZA)
      EQUIVALENCE (C(343), XDA)
      EQUIVALENCE (C(344), YDA)
      EQUIVALENCE (C(345), ZDA)
      EQUIVALENCE (C(346), CNCTS)
      EQUIVALENCE (C(347), FLGCTS)
      EQUIVALENCE (C(348), ERSAZ)
      EQUIVALENCE (C(349), ERSEL)
      EQUIVALENCE (C(356), CTHTS)
      EQUIVALENCE (C(357), STHTS)
      EQUIVALENCE (C(358), CPSIS)
      EQUIVALENCE (C(359), SPSIS)
      EQUIVALENCE (C(416), CL1YC)
      EQUIVALENCE (C(420), D1Y)
      EQUIVALENCE (C(423), CL1Z)
      EQUIVALENCE (C(427), D2Y)
      EQUIVALENCE (C(428), D2Z)
      EQUIVALENCE (C(431), DT)
      EQUIVALENCE (C(932), TLC)
      EQUIVALENCE (C(946), TLC)
      DATA RAD=57.29577955.0/
      IF (T.LT.TLC) GO TO 200
C     GIMBAL ANGLE LIMITS
      GMBLIM=14./RAD
      RXZA=SGRT(XDA**2+ZDA**2)
C     TRACKING RATE LIMIT
      TRLIM=2C./RAD
C     IF (RXZA.LE.RS) GO TO 10
C     FLAGS=C.     SIGNALS START OF SEARCH
C     FLAGS       SIGNALS SEEKER LOCKED AFTER SEARCH
      FLGCT=0      SIGNALS END CF SEARCH
C     FLGT=C.      SIGNALS END CF SEARCH
C     FLGGC=0.     SIGNALS DETECTION OF TARGET
C     FLAGLT=0.    SIGNALS TARGET OUTSIDE SEEKER FOV
      FLAGLT=0.
C     SEEKER POINTING ERRORS-ATIGS TARGET
      ELA=ATAN(-ZDA/XDA)
```

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```
C
      AZA=ATAN(YCA/RXZA)
C     KEEP SEEKER CAGED IF POINTING ERRORS EXCEED GIMBAL LIMITS
      ELA1=ELA-4./RAD
      AZA1=AZA-4./RAD
      IF (ABS(ELA1).GT.GMBLIM) GO TO 200
      IF (ABS(AZA1).GT.GMBLIM) GO TO 200
C     PRECESS SEEKER TO SEARCH INITIATION PT
      CMGYC=AKS*ELA1
      CMGZC=AKS*AZA1
      GO TO 90
C     SEARCH SEQUENCE
   10 IF (FLAGS.GT.0.0) GO TO 20
      TME=T
      FLAGS=1.0
      WRITE (6,150) RMA,T
   20 IF (FLGTS.GT.0.0) GO TO 75
      TS=T-TME
      IF (TS.GT.0.4) GO TO 30
      CMGYC=C.
      CMGZC=-10./RAD
      GO TO 90
   30 IF (TS.GT.1.35) GO TO 40
      CMGYC=C.
      CMGZC=10./RAD
      CMGC=ABS(CMGZC)
      GO TO 90
   40 IF (TS.GT.1.775) GO TO 50
      CMGYC=-TRLIM
      CMGZC=C.
      CMGC=ABS(CMGYC)
      GO TO 90
   50 IF (TS.GT.2.4) GO TO 60
      CMGYC=C.
      CMGZC=-TRLIM
      CMGC=ABS(CMGZC)
      GO TO 90
   60 IF (TS.GT.2.825) GO TO 65
      CMGYC=TRLIM
      CMGZC=C.
      CMGC=ABS(CMGYC)
      GO TO 90
   65 IF (TS.GT.3.425) GO TO 70
      CMGYC=C.
      CMGZC=TRLIM
      CMGC=ABS(CMGZC)
      GO TO 90
C     END OF SEARCH
```

```
   70 IF(FLGL.GT.0.0) GO TO 90
      OMGZC=0.0
      OMGYC=0.0
      WRITE(6,130)
      FLGTS=1.0
      GO TO 90
   75 IF(FLGL.GT.0.0) GO TO 80
      GO TO 90
C
C     REPOSITION SEEKER ON DETECTED TARGET
   80 IF(FLGT.GT.0.0) GO TO 85
      RYZT=SQRT(YDT**2+ZDT**2)
      OMGYC=-TRLIM*ZDT/RYZT
      OMGZC=TRLIM*YDT/RYZT
      IF(ANGLT.LE.0.25) FLGT=1.0
      GO TO 90
C
C     RADIOMETER AND SENSOR FILTER LAGS
   85 WSF=201.7
      DIYD=WSF*(2*ERSEL-DIY)
      DIZD=WSF*(2*ERSAZ-DIZ)
C
C     RECEIVER NOISE MODEL
      SGMNOIS=.C4815E-05*RMT*2.718282**(RMT*5.614624E-06)
      ELNOIS=.C2*SGMNOI*CACIS1
      AZNOIS=.C2*SGMNOI*CACIS2
C
C     ADD TO FILTERED RADIOMETER SIGNAL
      DIYN=DIY+ELNOIS
      DIZN=DIZ+AZNOIS
      OMYC1=WSF*(AKS*DIYN/RAD-OMYC1)
      OMZC1=WSF*(AKS*DIZN/RAD-OMZC1)
      OMGYCC=OMYC1
      OMGZCC=OMZC1
C
C     IF SEEKER LOSES TGT, PRECESSION COMMANDS GO TO ZERO
   88 IF(ABS(ANGLT).LE.2.5) GO TO 90
      IF(FLAGLT.GT.0.0) GO TO 90
      WRITE(6,140) ANGLT
      FLAGLT=1.0
C
C     SEEKER PRECESSION RATES
   90 IF(ABS(OMGYC).GE.TRLIM) OMGYC=SIGN(TRLIM,OMGYC)
      IF(ABS(OMGZC).GE.TRLIM) OMGZC=SIGN(TRLIM,OMGZC)
C
C     GIMBAL Y-AXIS ANG RATE TO SEEKER Y-AXIS
      OMGYR=CPSIS*SPSIS*(R*STHTS-P*CTHTS)
      OMGYR=OMGYR
C
C     SEEKER DYNAMICS
      D2Y2=2.4*(OMGYC-OMGYS)
      OMGYD=2139.*(U2Y+D2YC/64.3)
      D2ZD=4.4*(OMGZC-OMGZS)
      OMGZD=1445.625*(D2Z+D2ZD/64.3)
C
C     SEEKER EULER ANGLE RATES
      THTSD=OMGYS-G
```

```fortran
      PSISC=C*GZ-P*STHTS-R*CTHTS
      THTLIM=SIGN(GMBLIM,THTS)
      PSILIM=SIGN(GMBLIM,PSIS)
      IF(ABS(THTS).GT.GMBLIM)   THTSD=50.*(THTLIM-THTS)
      IF(ABS(PSIS).GT.GMBLIM)   PSISD=50.*(PSILIM-PSIS)
1200  RETURN
      FORMAT(1H ,10X,'END OF SEARCH,NO TARGET DETECTION')
130   FORMAT(1H ,10X,'SEEKER LOST TARGET,LOOK ANGLE=',F8.3)
140   FORMAT(1H ,10X,'START SEARCH,ATTGS,TGT RGE=',F10.3,3X,'T=',F8.3)
150   END
C
C
C
      SUBROUTINE S2I
C
      COMMON C(3415)
      EQUIVALENCE (C(0336),FLGD)
      EQUIVALENCE (C(0347),FLGTS)
      FLGD=0.0
      FLGTS=0.0
      RETURN
      END
C
C
      SUBROUTINE S2
C
      RADIOMETER MODULE  S2
C
      COMMON C(3415)
      EQUIVALENCE (C(0172),ETA02)
      EQUIVALENCE (C(0224),A11)
      EQUIVALENCE (C(0228),A12)
      EQUIVALENCE (C(0232),A13)
      EQUIVALENCE (C(0236),A21)
      EQUIVALENCE (C(0240),A22)
      EQUIVALENCE (C(0244),A23)
      EQUIVALENCE (C(0248),A31)
      EQUIVALENCE (C(0252),A32)
      EQUIVALENCE (C(0256),A33)
      EQUIVALENCE (C(0273),THTS)
      EQUIVALENCE (C(0277),PSIS)
      EQUIVALENCE (C(0280),ANGLT)
      EQUIVALENCE (C(0298),XTP)
      EQUIVALENCE (C(0298),YTP)
      EQUIVALENCE (C(0306),ZTP)
      EQUIVALENCE (C(0310),XTTP)
      EQUIVALENCE (C(0311),YTTP)
      EQUIVALENCE (C(0312),ZTTP)
```

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```
      EQUIVALENCE (CC(0031Z),XATP)
      EQUIVALENCE (CC(0031A),YATP)
      EQUIVALENCE (CC(0031S),ZATP)
      EQUIVALENCE (CC(0031G),RS)
      EQUIVALENCE (CC(0031V),FLGT)
      EQUIVALENCE (CC(0031B),RMT)
      EQUIVALENCE (CC(00319),XCTT)
      EQUIVALENCE (CC(0032Z),YCT)
      EQUIVALENCE (CC(00321),ZCT)
      EQUIVALENCE (CC(0035Z),FLAGS)
      EQUIVALENCE (CC(0033E),FLGD)
      EQUIVALENCE (CC(0034Z),X2)
      EQUIVALENCE (CC(00341),Y2)
      EQUIVALENCE (CC(00342),Z2)
      EQUIVALENCE (CC(00343),RMA)
      EQUIVALENCE (CC(00344),XCA)
      EQUIVALENCE (CC(00345),YDA)
      EQUIVALENCE (CC(00346),ZCA)
      EQUIVALENCE (CC(00347),CMCC)
      EQUIVALENCE (CC(00348),FLGTS)
      EQUIVALENCE (CC(00349),ERSAZ)
      EQUIVALENCE (CC(00356),ERSEL)
      EQUIVALENCE (CC(00357),CTLTS)
      EQUIVALENCE (CC(00358),CPSIS)
      EQUIVALENCE (CC(00359),SPSIS)
      EQUIVALENCE (CC(00932),T)
      EQUIVALENCE (CC(00946),TUC)

C     TARGET POSITION IN BODY AXIS SYSTEM
      XMT=A11*X1+A12*Y1+A13*Z1
      YMT=A21*Y1+A22*Y1+A23*Z1
      ZMT=A31*Y1+A32*Y1+A33*Z1
      RMT=SQRT(XMT**2+YMT**2+ZMT**2)

C     ATIGS...POSITION IN BODY AXIS SYSTEM
      XMA=A11*X2+A12*Y2+A13*Z2
      YMA=A21*Y2+A22*Y2+A23*Z2
      RMA=SQRT(XMA**2+YMA**2+ZMA**2)
      IF(...)GO TO 2C0

C     SEEKER DIRECTION COSINES WRT BODY (PITCH-YAW SEQUENCE)
      CTLTS=CC(TLTS)
```

```
      STHTS=SIN(THTS)
      CPSIS=COS(PSIS)
      SPSIS=SIN(PSIS)
      B11=CPSIS*CTHTS
      B12=SPSIS*STHTS
      B13=-CPSIS*STHTS
      B21=-SPSIS*CTHTS
      B22=CPSIS
      B23=SPSIS*STHTS
      B31=STHTS
C
      B32=0.0
      B33=CTHTS
C   RESOLVE TGT POSITION FROM BODY SYSTEM TO SEEKER AXES
      XDT=B11*XMT+B12*YMT+B13*ZMT
      YDT=B21*XMT+B22*YMT+B23*ZMT
      ZDT=B31*XMT+B32*YMT+B33*ZMT
      RYZT=SQRT(YDT**2+ZDT**2)
      RXYT=SQRT(XDT**2+YDT**2)
C   RESOLVE ATTICS TGT POSITION FROM BODY SYSTEM TO SEEKER AXES
      XCA=B11*XMA+B12*YMA+B13*ZMA
      YDA=B21*XMA+B22*YMA+B23*ZMA
      ZCA=B31*XMA+B32*YMA+B33*ZMA
      IF(FLAG0.GT.0.0) GO TO 5
      FLG1=0.0
      GO TO 20
    5 ANGLTR=ATAN(RYZT/XCT)
      ANGLT=ANGLTR*RAD
      IF(FLGTS.GT.0.0) GO TO 30
C   EFFECTIVE SEARCH BEAM WIDTH (DEG)
      BETA=6.2E-7-07-09*SQRT(CMGC*RAD/20.)*RMA**2
      BTAC2=BETA/2.0
C   TEST FOR TARGET DETECTION
      IF(FLG1.GT.0.0) GO TO 10
C   FLG1 SET WHEN TARGET ENTERS BEAM
      IF(ABS(ANGLT).LE.BTAC2) FLG1=1.0
      GO TO 20
   10 IF(FLG0.GE.1.0) GO TO 20
      TME=T
C   FLG0 SET WHEN TARGET LEAVES BEAM
      IF(ABS(ANGLT).GE.BTAC2) FLG0=1.0
      GO TO 20
   20 HD=T-TME
C   DETECTION DECLARED 30 MSEC AFTER TGT LEAVES BEAM
      IF(TD.GE.-0.03) GO TO 25
      GO TO 20
   25 IF(FLGTS.GE.1.0) GO TO 20
      WRITE(6,160) T
      FLGTS=1.0
```

```
      GO TC 200
30    IF(FLCGT.LE.0.0) GO TC 200
C     RADICMETER ERROR SIGNAL
      CHI1=2.*OIG3*(2.*ANGLT/3.-1.0)
      CHI2=2.*CI5*(2.*ANGLT/3.+1.0)
      IF((CHI1).EG.0.0) GO TC 4C
      ERSIG=(SIN(CHI1)/CHI1)**2-(SIN(CHI2)/CHI2)**2
      GO TC 50
40    ERSIG=1.0-(SIN(CHI2)/CHI2)**2
C     IF SEEKER LCSES TRACK
50    IF(ANGLT.GT.2.5) ERRCR SIGNAL=0.0
C     RESCLVE INTC AZ,EL ERRCR SIGNALS (SMALL ANGLE APPROX)
      IF(RYZT.LE.0.0) GC TC 6C
      ERSAZ=ERSIC*(YDT)/RYZT
      ERSEL=ERSIC*(-ZDT)/RYZT
      GO TC 2CCO
6C    ERSAZ=C.0
      ERSEL=C.0
200   RETURN
160   FORMAT (1H,10X,'END CF SEARCH,TARGET DETECTED.T=',F8.3)
      END
C
C
C
      SUBROUTINE S3I
      RETURN
      END
C
C
      SUBROUTINE S3
      RETURN
      ENC
C
C
      SUBROUTINE S4I
      RETURN
      END
C
C
      SUBROUTINE S4
      RETURN
      ENC
C
C
      SUBROUTINE S5I
      RETURN
      END
C
```

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```
      SUBROUTINE S5
C
C     ACCELEROMETERS AND GYROS MODULE
C
      COMMON (3415)
      EQUIVALENCE (CC(0136),CG)
      EQUIVALENCE (CC(0212),P)
      EQUIVALENCE (CC(0213),GC)
      EQUIVALENCE (CC(0216),RC)
      EQUIVALENCE (CC(0220),F)
      EQUIVALENCE (CC(0710),AX)
      EQUIVALENCE (CC(0711),AY)
      EQUIVALENCE (CC(0712),AZM)
      EQUIVALENCE (CC(1644),AZM)
      EQUIVALENCE (CC(1648),AYM)
      EQUIVALENCE (CC(1652),QM)
      EQUIVALENCE (CC(0980),RM)
      EQUIVALENCE (CC(1749),XAC)
      DATA (FLOAT/0.0/
C     ACCELEROMETER OFFSET FROM CC
C     ACCELEROMETERS AT STA. 134.5
      XACC=-4.9433
      XAX1=CX+XACC*(R**2+Q**2)
      AZ1=AZ+XACC*(R*P-QC)
      AY1=AY+XACC*(Q*P+RC)
      IF(FLOAT.GT.0.0) GO TO 10
C     IDEAL ACCELEROMETERS
      AX2=AX1
      AY2=AY1
      AZ2=AZ1
      GO TO 20
C     DIGITAL ACCELEROMETERS
C     TRANSFORMATION TO SKEWED ACCELEROMETER AXES
10    BA11=.BA11C12678
      BA12=.BA11C12678
      BA13=-.BA11C12678
      BA21=-.BA21
      BA22=C.BA11*BA21
      BA23=C.BA11*BA21
      BA31=BA11*BA21
      BA32=-C.BA21
      BA33=-C.BA11*BA21
      BAXA=BA11*AX1+BA12*AY1+BA13*AZ1
      AXA=BA11*AX1+BA12*AY1+BA13*AZ1
      AYA=BA21*AX1+BA22*AY1+BA23*AZ1
```

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```
C     AZA=EA31*AX1+BA32*AY1+BA33*AZ1
      ACCELEROMETER QUANT. STEF=.194 G
      AQS=6.*AXA/AGS
      ANSX=AXA/AGS*AINT(ANSX)
      ANSY=AYA/AGS*AINT(ANSY)
      ANSZ=AZA/AGS*AINT(ANSZ)
C     TRANSFORMATION BACK TO BODY AXES
      AXM=BA11*AXMA+BA21*AYMA+BA31*AZMA
      AYM=BA12*AXMA+BA22*AYMA+BA32*AZMA
      AZM=BA13*AXMA+BA23*AYMA+BA33*AZMA
C     ***** IDEAL GYROS *****
   20 GM=G
      RM=R
      FM=P
      RETURN
      END
C
C     SUBROUTINE S6I
      RETURN
      END
C
C     SUBROUTINE S6
      RETURN
      END
C
C     SUBROUTINE S7I
      RETURN
      END
C
C     SUBROUTINE S7
      RETURN
      END
C
C     SUBROUTINE S8I
      RETURN
      END
C
C     SUBROUTINE S8
      RETURN
```

```
      END
C
      SUBROUTINE SS1
      RETURN
      END
C
      SUBROUTINE SS
      RETURN
      END
C
      SUBROUTINE S101
      RETURN
      END
C
      SUBROUTINE S10
      RETURN
      END
CCC
C
      SUBROUTINE BCOST (TT,THRUST,FF)
C
      DIMENSION T(25),F(25),W(25)
      COMMON C(3415)
      EQUIVALENCE (C(0933),T1)
      EQUIVALENCE (C(9507),T)
C
      DATA T(1)/0.0/,T(2)/.075/,T(3)/.08/,T(4)/.10/,T(5)/.50/,T(6)/1.0/,
     1T(7)/1.50/,T(8)/1.75/,T(9)/1.95/,T(10)/2.125/,T(11)/3.125/,T(16)/3.95/,
     2T(12)/4.025/,T(13)/3.70/,T(14)/3.80/,T(15)/3.875/,T(20)/4.20/,T(21)/4.25/,
     3T(17)/4.025/,T(18)/4.15/,T(19)/4.15/,T(20)/4.60/,T(25)/4.75/,
     4T(22)/4.35/,T(23)/4.475/,T(24)/4.475/,T(25)/4.75/
C
      DATA F(1)/0.0/,F(2)/2000./,F(3)/16000./,F(4)/17800./,F(5)/19200./,
     1F(6)/21500./,F(7)/24100./,F(8)/25100./,F(9)/25800./,F(10)/26100./,
     2F(11)/26400./,F(12)/26400./,F(13)/26400./,F(14)/25600./,
     3F(15)/24800./,F(16)/24000./,F(17)/22000./,F(18)/16000./,
     4F(19)/9000./,F(20)/9000./,F(21)/6900./,F(22)/4900./,F(23)/1900./,
     5F(24)/900./,F(25)/0.0/
C
      DATA W(1)/0.0/,W(2)/.321/,W(3)/2.841/,W(4)/6.575/,W(5)/61.178/,
     1W(6)/111.759/,W(7)/148.810/,W(8)/172.301/,W(9)/182.143/,W(13)/376.037/,
     2W(10)/226.751/,W(11)/255.867/,W(12)/362.863/,W(16)/392.396/,W(17)/397.734/,
     3W(14)/381.512/,W(15)/388.351/,W(16)/392.396/,W(17)/397.734/
```

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```
      4W(18)/401.847/,W(19)/404.344/,W(20)/406.206/,W(21)/407.368/,
      5W(22)/408.356/,W(23)/409.175/,W(24)/409.883/,W(25)/410.296/

C
      TIME=TT-T1
      IF(TIME.GT.C.) GO TO 3
      FF = 0.0
      THRUST = C.0
      GO TO 4
    3 DO 1 I = 2,25
      IF(T(I).GE.TIME) GO TO 2
    1 CONTINUE
      CALL EXIT
    2 AK=(TIME-T(I-1))/(T(I)-T(I-1))
      THRUST=F(I-1) + (F(I) - F(I-1))*AK
      FF = W(I-1) + (W(I) - W(I-1))*AK
      PSF=2116.217*((1.C-(6.8753470E-06)*H)**5.25627005)
      THRUST=THRUST+(2116.2-PSF)*.715428
    4 RETURN
      END

CCC
CCCC  SUBROUTINE RAMJET (HIN,XMIN,AIN,WFIN,XIN,CT)
CCCC  SIMPLIFIED RAMJET MODEL
C     USES TABLE LOOK-UP FCR THRUST COEFF AND FUEL FLOW RATE

      DIMENSION TM1(6),TM2(7),TH(4),TETA(5),TCF1(6,5,4),TCF2(7,5,4),
     1TWF(6,5,4)
      COMMON C(3415)

C
      DATA TM1/2.3,2.5,2.7,2.9,3.1,3.3/
C
      DATA TM2/C.5,1.0,1.5,2.0,2.5,3.0,3.3/
C
      DATA TH/5C0.,13000.,2CCCC.,35000./
C
      DATA TETA/C.,2.,4.,6.,8./
C
      DATA TCF1/  .3814,.2958,.2075,.1374,
     A.0644,.C443,.1203,.2843,.3476,.2025,.1339,.0805,.0402,.3731,.2818,
     B.1915,.1203,.0666,.0451,.1001,.1595,.2526,.0201,.1655,.1049,.0555,.C173,
     C.C325,.2355,.1595,.4337,.1253,.2401,.1654,.1075,.4357,.3412,.2452,.1651,
     D.1114,.2287,.1512,.0927,.4485,.4012,.2967,.2061,.1350,.0639,.4273,.3268,
     E.2287,.1512,.0927,.1954,.1300,.0805,.0425,.4944,.386,.2798,.0810,.C3963,
     G.11641,.4924,.3172,.2742,.1924,.1256,.0832,.4857,.3706,.2618,
     H.1766,.1132,.066,.4572,.3376,.237,.1588,.1003,.056,.4328,.3186,
```

```
C
      DATA TCF2/-.5727,-.3661,-.4238,
     1 -.2254,.1535,.0999,.6273,.5135,.3661,.2997,.2243,.1661,
     2 .6252,.5028,.3911,.4721,.2562,.2202,.1616,.4598,.3801,.2821,.2054,
     3 .1451,.1542,.1398/

C
      DATA TWF/-.5727,-.3661,-.4238,
     ...

C
      IF(AIN.GT.CRUISE) GO TO 10
      RAMJET=TRRECL(XMIN,AIN,H,TN1,TETA,TH,TCF1,6,5,4)
      CT=TRRECL(XMIN,AIN,H,TN1,TETA,TH,TWF,6,5,4)
      GO TO 20
C
   10 RAMJET=TCFF CRUISE
      CT=TRRECL(XMIN,AIN,H,TN2,TETA,TH,TCF2,7,5,4)
      WFIN=0.0
   20 RETURN
      END
C
```

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```
      SUBROUTINE ENGINE (FIN,XFIN,AIN,WFIN,TIN,XIN,YIN,ZIN,CT,SMARG,
     1                   IFI,IREAD)
C
C     NWC COMMON DECK FOR AIRBREATHING PROPULSION PROGRAMS
C     CPIA NOMENCLATURE
C
      REAL ISF,ISTAR,M,M1,M2,M3,M4,M5,M6,MW,MW1,MW2,MW3,MW4,MW5,MW6
      REAL NACR,NACRS,MACH
      INTEGER CCLAT
C
      COMMON/CRLS/    ENG(30),IENG(15)
      COMMON /RJ/     A,AINF,A1,A2,A3,A4,A5,A6,AR,AFR,AFS,ALPHA
      COMMON /RJ/     ACR,BLEED
      COMMON /RJ/     CCASUP,CCASUB,CF,CFINF,CF6,CFB,CFT,CFC,CNM
      COMMON /RJ/     ERR,ERRL,ETAC,ETAN,F
      COMMON /RJ/     FAR,G,GAMMA,GAMMA1,GAMMA2,GAMMA3,GAMMA4,GAMMA5,GAMMA6
      COMMON /RJ/     HISP,ISTAR,I1,I2,I3,I4,I5,I6,I7,I8,I9,I10
      COMMON /RJ/     CCUNT,ICCNV,ICCNVP,IFIRST
      COMMON /RJ/     M,M1,MACR,MACRS,M2
      COMMON /RJ/     M4,M5,M6,MW,MW1,MW2,MW3,MW4,MW5,MW6
      COMMON /RJ/     P,P1,P2,P3,P4,P5,P6,PT30I,PRAR
      COMMON /RJ/     PT,PT1,PT2,PT3,PT4,PT5,PT6,PMOPT,PMOPT1,PMOPT2,PMOPT3
      COMMON /RJ/     PHI1,PHI2,PHI3,PHI4,PHI5,PHI6,PTI6,PT,PRI,G
      COMMON /RJ/     RADEG,R,SA,SART,SQPTOT
      COMMON /RJ/     T,T1,T2,T3,T4,T5,T6,TIME
      COMMON /RJ/     TT,TT1,TT2,TT3,TT4,TT5,TT6
      COMMON /RJ/     V,V1,V2,V3,V4,V5,V6
      COMMON /RJ/     WA,WF,X,Y,Z
C
      COMMON /EXHALS/ TABLE(1000)
C
      COMMON /WRITCT/ WRIT(20)
C
      NAMELIST /MCNT/ ENG,IENG
C
C     *** THE INFORMATION BELOW NOTES HOW THE NAMELIST
C     DATA IS INPUT AND WHAT THE INPUTS ARE ***
C
C     ENG(1)=A1/AR OR A1  (2 SQ)    SEE 16
C     ENG(2)=A3/AR OR A3  (2 SQ)    SEE 16
C     ENG(3)=A4/AR OR A4  (2 SQ)    SEE 16
C     ENG(4)=A5/AR OR A5  (2 SQ)    SEE 16
```

```fortran
C     ENG(5)=AE/AR OR A6 (M/SEC)          SEE I6
C     ENG(6)=AR (METRES SQUARED)
C     ENG(7)=CCE  BURNER DRAG COEFFICIENT
C     ENG(8)=ETAN, NOZZLE THRUST EFFICIENCY
C     ENG(9)=ETAC, COMBUSTION EFFICIENCY
C     ENG(10)=WFP, ISP STAR (FOR GAS GEN SYSTEMS)    SEE I5
C     ENG(12)=ELECTED FLOW PERCENTAGE/ 100 (AFS)
C     ENG(14)=AIR TO FUEL STOICHEMETRIC (AFS)
C     ENG(15)=CAN, NOZZLE MASS FLOW COEFFICIENT
C
      REAL MCCSE
      DIMENSION MCCSE(176), EAGLE(176)
C
C*** THE INPUTS BELOW ARE SWITCHES ***
C     IENG(1)=I1, ENGINE TYPE SWITCH
C       IF I1=0,RAMJET TYPE   IF I1=1, GAS GEN TYPE
C     IENG(2)=I2, COMBUSTION EFF SWITCH
C       IF I2=C, SET BY INPUT
C       IF I2=1, ETAC IS SET IN A SUBROUTINE
C     IENG(3)=I3, STANDARD ATMOSPHERE CHOICE SELECTION, SEE MEMO BY RGL
C     IENG(4)=I4, REAL AIR SWITCH
C       IF I4=C, GAMMA=1.4 REAL AIR SOLUTION
C       IF I4=1, USES THE       SOLUTION
C     IENG(5)=I5,          WF SWITCH IN THE SOLUTION
C       IF I5=1, FOR PROGRAM       WF SWITCH IN THE SOLUTION
C     IENG(6)=I6, THE INLET AREA   TYPE SWITCH
C       IF I6=C, THE AREAS ARE RATIOS BASED ON AR
C       IF I6=1, THE AREAS ARE ABSOLUTE VALUES
C     IENG(7)=I7, PRINT DEBUG DATA SWITCH
C       IF I7=0, DO NOT PRINT DEBUG DATA
C       IF I7=1, PRINT DEBUG DATA EACH ITERATION
C     IENG(8)=I8, COMBUSTION PRESSURE EFFECT SWITCH
C       IF I8=0, THERE IS NO PRESSURE EFFECT
C       IF I8=1, THE PRESSURE EFFECT ON COMBUSTION TEMP IS COMPUTED
C
      EQUIVALENCE(TABLE(206),MCOSF(1))
      EQUIVALENCE(TABLE(382),EAGLE(1))
C
C*** EXAMPLE OF NAMELIST INPUT ***
      $MCNT
      ENG=.5256,.65,.85,.4444,.56,.1140092,0.,.98,.65,2.,.50,1.2,.04,13.8
      IENG=C,0,2,C,1,C,0,0,
      $END
```

```
C     IF (IREAC.EQ.1) GO TC 10
C     COMMENT READ IN CATA AND RETURN TO CALLING ROUTINE
      READ (5,MCNT)
      WRITE (6,MCNT)
      RETURN
C     COMMENT PLT DATA IN FCRM THAT THE ATHODYC PRCGRAM CAN USE
   10 CCNTINUE
      MACH=C.C
      I=XHIN
      I2=XMIN
      ALFHA=AIN
      WF=WFIN
      TIME=TIN
      IF(WFIN.LT.0.0001.ANC.TIME.GT.20.) IFUEL=4
      IFIRST=IFI
C                              X=XIN       @ GAMMA
C                              Y=YIN       @ NOT USEC
C                              Z=ZIN       @ NOT USEC
      Z=ZIN
      A1=ENG(1)
      IF(TIME.LT.10.0) A1=.43244
      IF(TIME.GT.1C.0.AND.TIME.LT.50.0) A1=.43162+.00008639*TIME
      IF(TIME.GE.50.0) A1=.43594
      A3=ENG(2)
      A4=ENG(3)
      IFLUEL=0
      IF(XHIN.GE.1.0) IFUEL=5
      IF(TIME.LE.12.5) A5=.5C326
      IF(TIME.GT.12.5.ANC.TIME.LE.40.) A5=.51410+.00023829*TIME
      IF(TIME.GT.4C..AND.TIME.LE.66.) A5=.51776+.00014694*TIME
      IF(TIME.GT.66.) A5=.52746
      A6=ENG(4)
      AR=ENG(5)
      CCE=ENG(7)
      ETAN=ENG(9)
      ETAC=ENG(6)
      IF(IEAC(1).EQ.2) WF=ENG(10)
      ISTAR=ENG(11)
      PHIPRI=ENG(12)
      ELEC=ENG(13)
      AFS=ENG(14)
      CNM=ENG(15)
      IF (CNM.LT.0.5) CNM=1.0
      I1=IENG(1)
      I2=IENG(2)
```

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```
      I3=IENG(3)
      I4=IENG(4)
      I5=IENG(5)
      I6=IENG(6)
      I7=IENG(7)
      I8=IENG(8)
      IF(I3.EQ.0) A1=A1*AR
      IF(I4.EQ.0) A3=A3**AR
      IF(I5.EQ.0) A4=A4**AF
      IF(I6.EQ.0) A5X=A5*AR
      IF(I6.EQ.0) A6=A6**AF
      IF(I6.EQ.1) A5X=A5
      A5=A6X*AR
      IF(IFIRST.EQ.-1) GO TO 20
      GO TO 20
   20 CONTINUE
C     INITIALIZE ,SET CONSTANTS AND WRITE AREAS
C
C     AIRBREATHING GEOMETRY
C     CALCULATE GEOMETRY PARAMETERS ONLY CALLED ON FIRST PASS

      A40A5=A4/A5
      GAM=5.0/7.0
      M4=FNARL(GAM,A40A5)
      PHI4=PTIN(GAM,M4)
      A6CA5=A6/A5
      M6=FNARH(GAM,A60A5)
      PHI6=PTIN(GAM,M6)
C
C     IDENTIFY AND PRINT PARAMETERS
C
      WRITE(6,420) A1
      WRITE(6,430) A3
      WRITE(6,440) A4
      WRITE(6,450) A5X
      WRITE(6,460) A6
      WRITE(6,470) AR
      WRITE(6,480) PHI4
      WRITE(6,490) PHI6
      WRITE(6,500) CDB
      WRITE(6,520) CNM
   20 CONTINUE
C
C     SET CONSTANTS AND INITIALIZE SUBROUTINES
C     G IN KG M/SEC SQ - N
```

```
C       RADEG=.5725577779E+02
        G=5.6666E

C       START CALCULATIONS FOR EACH NEW POINT

        COUNT=0
        ICCNVP=1

C       NEW ITERATIONS START HERE

40      ICCNV=C

C       CHECK TO SEE IF 100 ITERATIONS OF THE SAME POINT HAVE BEEN MADE

C       IF (COUNT-100) 60,60,50

C       IF NOT CONVERGED AFTER 100 ATTEMPTS, STOP

50      WRITE (6,520)

C       CALL EXIT
C       IF NOT CONVERGED WITH LESS THAN 100 ATTEMPTS, TRY AGAIN

60      CONTINUE
        IF(COUNT.GT.89) I7=1C
C       IF ABCVE STATEMENT NOT CONVERG,PRINT LAST 10
        IF (COUNT.NE.0) GO TC 90 CALL AIR(H,M,-1,P,T,A,DEN,Q,G,1,1)
        IF (IFIRST.EG.-1) CALL AIR(H,M,-1,P,T,A,DEN,Q,G,1,1)
        IF (IFIRST.EG.-1) GO TC 70
        I3=I3+100
        CALL AIR(H,M,1,P,T,A,DEN,Q,G,1,1)
70      G=5.8066
        IF (I4.EG.1) GO TO 8C

C       ENTHR IN CAL/GM
        ENTHR=6.4278+.2394*(T-194.444)

C       V IN METRES PER SEC
        V=M*A

C       ENERG IN CAL/GM
        ENERG=(V**2.)/8368.
        ENTHAL=ENTHR+ENERG

C       ECGM IN CAL/GM
        ECGM=ENTHAL+ENERG

C       TT3 IN DEGREE RANKINE
        TT3=535.31+(7.5164*ECGM)-(3.3559E-03*ECGM*ECGM)+(4.6597E-06*(ECGM
       1**3.))-(1.3295E-09*(ECGM**4.))
        TTE=TT3/1.8
        GAMMA3=1.4048-(6.09654E-04*ECGM)+(2.12102E-06*ECGM*ECGM)-(5.56845E
```

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```
      1-05*(ECCM**2.))+(6.45543E-12*(ECGM**4.))
      GO TC 90
 80   CONTINUE
      GAMMA3=1.4
      TT3=T/FTICTT(1.4,M)
      T3=TT3*FTICTT(1.4,M3)
 90   CCNTINUE
C
 100  IF (IFIRST) 100,110,110
      WRITE (6,540)
C
C     COMBLSTCR
C
      IF (I2.EC.1) CALL ETA
      CALL TAE (AFS)
      V=-0.0
      WA=1C.C
      M3=.N
      WACRS=1.CRA
      CALL HCRA
C
C     CALCLLATICN
C
      WRITE (6,230)
C
C     DIFFLSER
C
      CALL HCF
      GO TC 150
 110  CONTINUE
      IF (N.GT.1.07) GO TC 130
C     ****** BEGIN SUBSONIC CALL SEQUENCE ******
      IF (WF.LT..001) GO TC 120
      PT=P/FFCPT(1.4,M)
      FMOPT=FFNCPT(1.4,M)
      TT=T/FTICTT(1.4,M)
      ACR=.2781+2.4721*N-4.527*M*M+2.3036*M*M*M
      AINF=A1*ACR*1.05
      WA=(AINF*FT*FMOPT)/SGRT(TT)
      CALL HCRA
 120  CONTINUE
      IF (WF.LT..001) ER=9.9
      FAR=ER/AFS
      CALL SLESCN (H,M,FAR,CF,WF,Q,AR)
      ICCNV=C
      COUNT=C
      GO TC 25
C     ****** ENC OF SUBSCNIC CALL SEQUENCE ******
```

```
130 CONTINUE
C
C ******** WE SET SA HERE *********
C
      IF (I5.EG.1) GO TO 140
      IF (I5.EG.2) GO TO 150
      WRITE (6,240)
C GO THIS ROUTE IF ER IS INPUT OR CHANGED IN HCRA
140   CONTINUE
      CALL HCRA
      IF(IFUEL.EG.5) ER=0.0
      FAR=ER/AFS
      WF=FAR*WA
      AFR=1./FAR
      GO TO 160
C GO THIS ROUTE IS WF IS INPUT OR SET IN HCRA
150   CONTINUE
      CALL HCRA
      IF(IFUEL.EG.5) WF=0.0
      FAR=WF/WA
      ER=FAR*AFS
      IF(FAR.EG.0.0) GO TO 1400
      AFR=1./FAR
      GO TO 160
1400  AFR=0.0
C
160   CONTINUE
C
      TOTT3=FTCTT(GAMMA3,N3)
      T3=TT3*TCTT3
      SQRTCT=SGRT(TT3)
C
C TO FIND AIR SPECIFIC IMPULSE
C
      IF(I10.EG.0) GO TO 161
      CONTINUE
      GO TO 165
161   CONTINUE
      CALL INTR20 (TT3,ER,TT4I,TABLE,1)
      CALL INTR20 (TT3,ER,GAMA4,TABLE,2)
      CALL INTR20 (TT3,ER,NW4,TABLE,3)
C
C COMPUTE THE EFFECT OF PRESSURE ON TEMPERATURE
C
      IF(I8.EG.0) GO TO 162
      G1=GAMA4+1.0
      G2=GAMA4-1.0
      G3=G1/G2
```

```
      G4=2.*G1*((2./G1)**G3)
      G5=SGRT(G4)
      FT4=(S4*WA)/(G5*A5)
      PT4ATM=FT4/101360.
      IF(PT4ATM.LT..2) PT4ATM=.2
      IF(PT4ATM.GT.20.) FT4ATM=20.
      IF(TT3.LT.255.) GO TO 1615
      IF(CER.GT.1.5) GO TO 1615
      CTEMF=TC(TT3,ER,PT4ATM)
 1615 CONTINUE
      TT4I=TT4I+CTEMP
  162 CONTINUE
C
C NCW FINISH COMBUSTOR COMPUTATIONS
C
      R=8314./NW4
      WAX=WA/.45=5924
      THROAT=((TT3*1.8)/1000.)**2.
      TTT=(WA)*T(TT)/THRCAT
      ESV=(WA)*EG.1) CALL ETA
      IF(IVEG.EC.1) CALL ETA
      TT4=ETA(A*R*(TT4I-TT3)+TT3
      BBB=2.*CC*R*(400.+GAMMA4)*TT4/GAMMA4
      BBB=2.*AAX1(400.,BBB)
      SA=(1.0+FAR)*SQRT(BEE)
      SART=SA/SQRTCT
  165 CONTINLE
C
C MMENT MAKE CALCULATIONS TAKING VARIABLE NOZZLE GAMMA INTO EFFECT
C
      A4CA5=A4/A5
      M4=FMARL(GAMMA4,A40A5)
      PHI4=PHIN(GAMMA4,M4)
C
C ***** WE COMPUTE CONDITIONS AT STATION 3 HERE ********
C
      STROG=23.9613
      IF(T11.EQ.1) GO TO 17C
C RANJET=STFCC=COMPUTATIONS - FUEL ADDED IN THE INLETS
      SARTA=STFCC*SQRT((GAMMA3+1.)/GAMMA3)*(1.+FAR)
      PHI3=(FH14*SQRT/SARTA)+(GAMMA3*CDB*M3*N3)/(2.*XMCIR3*SARTA))
      GO TC 18CC
C GAS GENERATOR SYSTEM COMPUTATIONS
  170 SARTE=STFCG*SQRT((GAMMA3+1.)/GAMMA3)
      PHI3=(PHI4*SART/SARTB)-((PHIPRI*ISTAR*FAR)/(SARTB*SQRTOT))+((GAMMA
     13*CDB*M3*M3)/(2.*XMCIR3*SARTB))
  180 CONTINLE
      M3=FAPHIN(GAMMA3,PHI3)
```

```
      FMCFT3=FMCFT(GAMMA3,M3)
      PMOPT=FMCPT(1.4,M)
      XMCIF3=FMCIR(GAMMA3,M3)
C ******** WE NOW CALL THE INLET ROUTINE TO GET WA *********
C
      CALL HCF
C 190 CONTINUE
C
C ******** DEBUG OUTPUT *********
      IF (I7.EC.0) GO TO 200
  201 CONTINUE
      F1K=P1/10000.
      F1K=F1/10000.
      F2K=F2/10000.
      P3K=P3/10000.
      P4K=P4/10000.
      P5K=P5/10000.
      P6K=P6/10000.
      PTK=PT/10000.
      PT1K=PT1/10000
      PT2K=PT2/10000
      PT3K=PT3/10000
      PT4K=PT4/10000
      PT5K=PT5/10000
      PT6K=PT6/1000
      QK=Q/10000.
      WRITE (6,250) A,AINF,A1,A2,A3,A4,A5,A6,AR,AFR,AFS,ALPHA
      WRITE (6,260) ACR,BLEEC
      WRITE (6,270) CDASUB,CDASUP,CDB,CF,CFINF,CF6,CFB,CFT,CFC,CNM
      WRITE (6,280) ER,ERRL,ERLL,ETAC,ETAN,F
      WRITE (6,290) FAR,G,GAMMA,GAMMA1,GAMMA2,GAMMA3,GAMMA4,GAMMA5,GAMMA
     16
      WRITE (6,300) H,ISP,ISTAR,I11,I12,I3,I4,I5,I6,I7,I8,I9,I10
      WRITE (6,310) COUNT,ICCAV,ICONVP,IFIRST
      WRITE (6,320) M1,M2,M3,M4,M5,M6,MW,MW1,MW2,MW3,MW4,MW5,MW6
      WRITE (6,330) MACR,MACRS,PM
      WRITE (6,340) PK,PIK,P2K,P3K,P4K,P5K,P6K,PT3CI,FRAR
      WRITE (6,350) PTK,PT1K,PT2K,PT3K,PT4K,PT5K,PT6K,PMOPT,PMCPT1,PMCFT
     12,PMCPT3
      WRITE (6,360) PHI1,PHI2,PHI3,PHI4,PHI5,PHI6,PHIPRI,QK
      WRITE (6,370) RADEG,F,SA,SART,SQRTOT
      WRITE (6,380) TT,TT1,TT2,TT3,TT4,T5,T6,TIME
      WRITE (6,390) TT,TT1,TT2,TT3,TT4,TT5,TT6
      WRITE (6,400) V,V1,V2,V3,V4,V5,V6
      WRITE (6,410) WA,WF,X,Y,Z
```

```
C
C  200  CONTINUE
C         SET IFTS, INCREASE COUNT AND CALCULATE PARAMETERS NOT IN COMMON
C
C         COUNT=COUNT+1
C
C         CHECK CONVERGENCE, ICCNVF IS USED TO MAKE SOLUTION CONVERGE TWICE
C         IF CONVERGED, PRINT.  IF NOT, GO BACK AND TRY AGAIN
C
       IF (IFIRST.EQ.-1) GO TO 225
       IF (ICCNVF+ICCNVP) 210,220,210
  210  ICCNVF=ICCNV
       GO TO 40
  220  CONTINUE
C******  WE NOW COMPUTE THRUST IF CONVERGED  ********
C
       A6CA5=A6/A5
       M6=FMARH(GAMMA4,A6CA5)
       PHI6=PFIN(GAMMA4,M6)
       IF(I10.GE.5) GO TO 221
       CF6=(WA4*PHI6*ETAN-A6*F)/(AR*Q)
  221  CONTINUE
       CCFINF=2.*ACR*MACRS*A1/AR
       CALPHA=CCS(ALPHA/RACEG)
       CF=CF6-((CFINF*CALPHA)+CFB+CFC
       F=CF*G*AR
       IF(WF.EQ.0.0) GO TO 1300
       ISP=F/(WF*G)
       GO TO 1500
 1300  ISP=C.C
 1500  CONTINUE
       G1=GAMMA4+1.C
       G2=GAMMA4-1.0
       G3=G1/G2
       G4=2.*G1*((2./G1)**G3)
       G5=SGRT(G4)
       PTE=(SA*WA)/(G5*A5)
C
C         PREPARE DATA FOR TRANSFER TO MAIN PROGRAM
C
  225  CONTINUE
       HIN=H
       XMIN=M
       AIN=ALFHA
       WFIN=WF
       CDADC=CDASUB+CDASUP+CFT
       CT=CF-CDACC
```

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      SMARG=FN
      IFI=IFIRST
      FCCUNT=FCCUNT+.01
      WRITE(1)=PT5CI
      WRITE(2)=WA
      WRITE(4)=TT4
      WRITE(5)=ZACR
      WRITE(6)=RACR
      WRITE(7)=ISP
      WRITE(8)=EERSP
      WRITE(9)=FCCUNT
      WRITE(10)=ETAC
      WRITE(11)=CT
      WRITE(12)=FN
      WRITE(14)=FCCUNT
      IF(PT3.EG.C.C)GO TO 1200
      WRITE(15)=FT5/PT3
 1200 CONTINUE
      WRITE(16)=PT5/1000.
      FCCUNT=FCCUNT
      RETURN
C
 2300 FORMAT(' COMPUTE PH13')
 2400 FORMAT(1H1,F8.2,8F7.4,2F7.3,F7.2)
 2500 FORMAT(' IS IS CUT CF RANGE-WHY')
 2600 FORMAT(2F8.5)
 2700 FORMAT(1CF8.5,F10.3)
 2800 FORMAT(6F8.5,F10.3)
 2900 FORMAT(F9.2,2F8.3,1CI2)
 3000 FORMAT(4I4,7F8.4)
 3100 FORMAT(7F7.4,7F8.4)
 3200 FORMAT(7F10.2,2F7.5)
 3300 FORMAT(7F10.2,4F7.5)
 3400 FORMAT(6F10.2)
 3500 FORMAT(7F10.5,F10.2)
 3600 FORMAT(5F10.5,2F8.5)
 3700 FORMAT(7F10.3)
 3800 FORMAT(7F10.3)
 3900 FORMAT(7F10.3,3F10.5)
 4000 FORMAT(54H1 AIR BREATHING ENGINE GEOMETRY)
 4100 FORMAT(14H A 1 = F9.7,9H SQ METRE)
 4200 FORMAT(14H A 2 = F9.7,9H SQ METRE)
 4300 FORMAT(14H A 3 = F9.7,9H SQ METRE)
 4400 FORMAT(14H A 4 = F9.7,9H SQ METRE)
```

```
470 FORMAT (14H    A 6  = F9.7,9H SQ METRE)
480 FORMAT (14H    AR   = F9.7,9H SQ METRE)
490 FORMAT (28H    PT14          = F7.5)
500 FORMAT (28H    PTI6          = F7.5)
510 FORMAT (28H    BURNER DRAG COEFF. = F6.2)
520 FORMAT (28H    NOZZLE MASS COEFF. = F6.2)
540 FORMAT (36H DID NOT CONVERGE AFTER 100 ATTEMPTS)
    FORMAT (47H0 RAMJET PROPULSION                        )

    END

    SUBROUTINE ETA

C   NWC COMMON DECK FOR AIRBREATHING PROPULSION PROGRAMS
C   CPIA NOMENCLATURE

    REAL ISF,ISTAR,M,M1,M2,M3,M4,M5,M6,MW,MW1,MW2,MW3,MW4,MW5,MW6
    REAL MACR,MACRS,ALPHA
    INTEGER COUNT

    COMMON /RJ/ A,AINF,A1,A2,A3,A4,A5,A6,AR,AFR,AFS,ALPHA
    COMMON /RJ/ ACR,BLEED
    COMMON /RJ/ CDASUB,CDASUF,CDB,CF,CFINF,CF6,CFB,CFT,CFC,CNM
    COMMON /RJ/ ER,ERRL,ERLL,ETAC,ETAN,F
    COMMON /RJ/ FAR,G,GAMMA,GAMMA1,GAMMA2,GAMMA3,GAMMA4,GAMMA5,GAMMA6
    COMMON /RJ/ ISP,ISF,ISTAR,I1,I2,I3,I4,I5,I6,I7,I8,I9,I10
    COMMON /RJ/ COUNT,ICONV,ICAV,ICR,IFIRST
    COMMON /RJ/ M,M1,M2,M3,M4,M5,M6,MW,MW1,MW2,MW3,MW4,MW5,MW6
    COMMON /RJ/ MACR,MACRS,PZ
    COMMON /RJ/ P,P1,P2,P3,P4,P5,P6,PT301,PRAR
    COMMON /RJ/ PT,PT1,PT2,PT3,PT4,PT5,PT6,PMOPT,PMOPT1,PMOPT2,PMOPT3
    COMMON /RJ/ PHI1,PHI2,PHI3,PHI4,PHI5,PHI6,PHIPRI,Q
    COMMON /RJ/ RADEG,R,SA,SQRTOT
    COMMON /RJ/ T,T1,T2,T3,T4,T5,T6,TIME
    COMMON /RJ/ TT,TT1,TT2,TT3,TT4,TT5,TT6
    COMMON /RJ/ V,V1,V2,V3,V4,V5,V6
    COMMON /RJ/ WA,WF,X,Y,Z

    DATA A11,E11,C11,D11,E11,F11,G11
   * /-14C(46,  .95416,  -8.55033, 43.7266, 1468.91,  80484.,
   * -277C56./

    FAR2=FAR*FAR
    FOVER=1./(1.+FAR)
```

```
      TERM1=E11+C11*FAR+D11*FAF2
      TERM2=E11+F11+FAR+G11*FAF2
      TTR=1.+E11*TT TERM1+FCVER*TERM2
      STT4I=SQRT(TT4I)
      ETAC=40.246*STT4I-0.3513*TT4I-1055.08
      ETAC=ETAC/ICC
      IF(ER.LT..0001) ETAC=0.0
      RETURN
      END
C
C
      SUBROUTINE HCRA
C
      DIMENSION FS(66), PSTAT1(11), FUELF(11)
C
C     NWC COMMON DECK FOR AIRBREATHING PROPULSION PROGRAMS
C     CPIA NOMENCLATURE
C
      REAL ISP,ISTAR,M,M1,M2,M3,M4,M5,M6,MW,MW1,MW2,MW3,MW4,MW5,MW6
      REAL MACR,MACRS
      INTEGER CCUNT
C
      COMMON /RJ/ A,AINF,A1,A2,A3,A4,A5,A6,AR,AFR,AFS,ALPHA
      COMMON /RJ/ ACR,BLEED
      COMMON /RJ/ CDASUB,CDB,CF,CFINF,CF6,CFB,CFT,CFC,CAM
      COMMON /RJ/ CDASUF,ETAC
      COMMON /RJ/ ERLL,ETAC,ETAN,F
      COMMON /RJ/ FAR,G,GAMMA,GAMMA1,GAMMA2,GAMMA3,GAMMA4,GAMMA5,GAMMA6
      COMMON /RJ/ I,ISP,ISTAR,I1,I2,I3,I4,I5,I6,I7,I8,I9,I10
      COMMON /RJ/ CCUNT,ICCAV,ICCNVP,IFIRST
      COMMON /RJ/ M,M1,M2,M3,M4,M5,M6,MW,MW1,MW2,MW3,MW4,MW5,MW6
      COMMON /RJ/ MACR,MACRS,PW
      COMMON /RJ/ P,P1,P2,P3,P4,P5,P6,PT30I,PRAR
      COMMON /RJ/ PT,PT1,PT2,PT3,PT4,PT5,PT6,PMOPT,PMOPT1,PMOPT2,PMOPT3
      COMMON /RJ/ PHI,PHI1,PHI2,PHI3,PHI4,PHI5,PHI6,PTIPRI,Q
      COMMON /RJ/ RADEG,R,SAR,SQRTOT
      COMMON /RJ/ TT,TT1,TT2,TT3,TT4,TT5,TT6,TIME
      COMMON /RJ/ V,V1,V2,V3,V4,V5,V6
      COMMON /RJ/ WA,WF,X,Y,Z
C
C     ANGLE OF ATTACK   PS(I)  I=3,14
C     MACH NUMBER       PS(I)  I=15,81
C
      DATA PS/
```

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```
      A12.0,.4,.0,.0,.0,.5,1.0,1.5,2.0,
      A2.,.4,.5,.6,.7,.8,.9,1.0,2.0,
      A1...,...,...,...,.89727,,.88386,,
      A...,.84808,,.89504,,.85721,,.88275,,
      A...,.93782,,.93504,,.89465,,.88165,,
      A...,.97145,,.93410,,.89314,,.87833,,
      A...,.97058,,.93038,,.89087,,.87501,,
      A...,.96120,,.92158,,.88871,,.87058,,
      A...,.95704,,.92104,,.87778,,.86842,,
      A...,.95670,,.91044,,.86076,,.84185,,
      A...,.95406,,.85257,,.83781,,.81745,,
      A...,.94111,,.87331,,.81180,,.78210,,
      A...,.92901,,.82267,,.79190,,.75666/
C
C     DATA FSTAT1/3.07,3.5,4.9,6.02,7.,8.,9.1,10.,11.,12.,13.18/
C
      DATA FUELF/.94,1.130,1.375,1.628,1.859,
      A2.056,2.250,2.416,2.562,2.722,3.05/
C
   10 IF (IFIRST) 10,20,20
      WRITE(6,50)
      RETURN
   20 CONTINUE
      IF (COUNT-1) 30,30,40
   30 CONTINUE
      CALL INTRPC (ALPHA,N,PSICP,PS,1)
      PSI=PSICP*(P/6894.757)
      TFFPS=COLI*(PSI,PSTAT1,FUELF,11)
      TFFPS=TFFPS*.4535924
      WF=TFF
      RETURN
   50 FORMAT (T6,'FUEL CONTROL FOR STV G         ')
C
      END
C
CCC
C     SUBROUTINE HCF
C
      DIMENSION PR(81), AA(81), CADD(12), XM(12), BWR(12)
CCC
CCC   AWC COMMON DECK FOR AIRBREATHING PROPULSION PROGRAMS
C     CPIA NOMENCLATURE
```

```fortran
      REAL ISP,ISTAR,M,M1,M2,M3,M4,M5,M6,MW,MW1,MW2,MW3,MW4,MW5,MW6
      REAL MACR,MACRS
      INTEGER CCUNT
C
      COMMON /RFJ/ A,AINF,A1,A2,A3,A4,A5,A6,AR,AFR,AFS,ALPHA
      COMMON /RFJ/ ACR,BLEED,...
      COMMON /RFJ/ CDASUB,CDASUP,CDB,CF,CFINF,CF6,CFB,CFT,CFC,CNM
      COMMON /RFJ/ ERR,ERRL,ETAC,ETAN,F
      COMMON /RFJ/ FAR,G,GAMMA,GAMMA1,GAMMA2,GAMMA3,GAMMA4,GAMMA5,GAMMA6
      COMMON /RFJ/ H,ISP,ISTAR,I1,I2,I3,I4,I5,I6,I7,I8,I9,I10
      COMMON /RFJ/ CCUNT,IC,ICNV,ICNVP,IFIRST
      COMMON /RFJ/ M,M1,MACR,MACRS
      COMMON /RFJ/ M2,M3,M4,M5,M6,MW,MW1,MW2,MW3,MW4,MW5,MW6
      COMMON /RFJ/ P,P1,P2,P3,P4,P5,P6,PT3OI,PRAR
      COMMON /RFJ/ PT,PT1,PT2,PT3,PT4,PT5,PT6,PMOPT,PMOPT1,PMOPT2,PMOPT3
      COMMON /RFJ/ PHI1,PHI2,PHI3,PHI4,PHI5,PT6,PHI6,PT,PRI,Q
      COMMON /RFJ/ RADEG,R,SA,SQRTOT
      COMMON /RFJ/ T,T1,T2,T3,T4,T5,T6,TIME
      COMMON /RFJ/ TT1,TT2,TT3,TT4,TT5,TT6
      COMMON /RFJ/ V,V1,V2,V3,V4,V5,V6
      COMMON /RFJ/ WA,WF,X,Y,Z
C
C     PRESSURE RECOVERY INSTALLED ALVJ -- BETA=0.0   (PS(I) I=19,81)
C
      DATA FR/
     A5=0,0,0,9,1.0,1.5,2.2,
     A2=2.7,4.0,6.0,10.0,1.0,2.0,
     A4
     A .9500000, .9400, .9250, .8775, .8320,
     A .9500000, .9450, .9250, .8775, .8320,
     A .9475, .9450, .9300, .8775, .8150,
     A .7660, .7600, .9100, .8600, .6575,
     A .6840, .6800, .7400, .7000, .5275,
     A .6350, .6300, .6350, .5750, .3800,
     A .3760, .3725, .4925, .4300, .2400,
     A .1925, .1650, .3400, .2850, .0800/
     A .3800, .2000, .1600, .1050,
C
C     AIR CAPTURE INSTALLED ALVRJ DEC 1975   AA(I) I=19,81
C
      DATA AA/
     A5=0,0,0,9,1.0,1.5,2.2,
     A2=2.7,4.0,6.0,10.0,1.0,2.0,
     A4=.9465,.9457,.9452,.9440,.9400,.9350,.9270,
     A .9465,.9457,.9452,.9440,.9400,.9350,.9270,
```

```
C     A   .5825,.5819,.5812,.5800,.5700,.5650,.5050,
      A   .6725,.6712,.6700,.6675,.6520,.6400,.6275,
      A   .5010,.5000,.8990,.8570,.8725,.8550,.8550,
      A   .5420,.5400,.9375,.9325,.9200,.9075,.9125,
      A   .5450,.5437,.9425,.9400,.9370,.9225,.9250,
      A   .5450,.5437,.9425,.9400,.9370,.9325,.9250/
C
      CATA XM/
      A   .5,.5,1.,1.4,1.6,2.2,2.43,2.48,2.5,2.7,3.0,3.25/
C
      CATA CALL/
      A   .0213,.0213,.0132,.125,.0988,.0221,.0184,.0173,.0171
      B   ,.0123,.0145,.0176/
C
      CATA BMR/
      A   .0339,.0339,.0208,.0227,.0245,.0334,.0287,.0265,.0255,
      B   .0213,.0171,.0150/
C
      1C  IF (IFIRST) 10,20,20
      10  CONTINUE
          PRAR=0.0
          TCL=.0004
          WRITE (6,100) TOL
          RETURN
C
      20  CONTINUE
C
C     SET PRESENT PR/AR EQUAL TO PREVIOUS PR/AR
C
          PRARP=PRAR
C
C     CALCULATE NEW PR/AR
C
          TT=T/FT(TT(1,4,M)
          TTRATC=SQRT(TT3/TT)
          PRAR=TTRATC*FMOPT*MACRS*A1/(PMOPT3*A3)
          IF (IBC.EQ.0) PRAR=TTRATC*PMOPT*MACRS*A1*(1.0+FAR)/(PMOPT3*A3)
C
C     CHECK FOR CONVERGENCE BY COMPARING PR/AR TO PREVIOUS PR/AR
C
          IF (AES(PRARP-PRAR)-TCL) 40,40,30
      30  ICGNV=1
      4C  CONTINUE
          CALFA=CCS(ALPHA/RAEEG)
C
```

```
C
C  COMPUTE CRITICAL PRESSURE RECOVERY AND MAXIMUM AIR CAPTURE RATIO
C
      ALPHAE=AES(ALPHA)
      CALL INTRZO(M,ALPHAE,MACR,AA,1)
      BLCCDE=.015
      BLEEDC=BLCDTS+BLDDB
      MACRS=MACR*(1.0-BLEEC)
      CALL INTRZO (M,ALPHAE,PRIAD,PR,1)
C
C  CRITICAL PRESSURE RECOVERY
C
      PACR=PRIAD
      IF (FRAR-PACR) 50,60,70
C
C  PRESSURE RECOVERY .LT. CRITICAL
C
   50 PT3CI=PRAR
      ACR=1.
      GO TO 80
C
C  PRESSURE RECOVERY .EQ. CRITICAL
C
   60 PT3CI=PRIAD
      ACR=1.
      GO TO 80
C
C  PRESSURE RECOVERY .GT. CRITICAL --CHANGE AIR CAPTURE AND SET PRES
C  RECOVERY EQUAL TO CRITICAL VALUE
C
   70 PT3CI=PRIAD
      ACR=PRIAD/FRAR
   80 POPT=PRCPT(1.4,M)
      PT=F/PCPT
      PT1=FT*PT3CI
      FM=(PRIAC-PT3CI)/(PRIAC/100.)
      AINF=ACR*A1*MACRS
      SQTINF=SQRT(TT)
      WA=(AINF*FT*FMOPT)/SQTINF
      IF(ICGNVF.NE.0 .OR. ICCNV.EG.1) RETURN
      CDSUB=C.0
      IF (FRAR.LE.FACR) GO TO 50
C
C  CALCULATE ADDITIVE CRAG DUE TO SUBSONIC SPILLAGE
C
      ETASUB=M/((M*10.2095)-11.5652)
      CDSUB=2.*(1.-ETASUB)*(1.-ACR)
```

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```
C     CALCULATE ADDITIVE DRAG DUE TO SUPERSONIC SPILLAGE
C
90    CAEC=CDLI(A,XM,CACC,12)
      IF(PRAR.LE.PACR)CDSLB=C.0
      CCASUB=CCSUB*A1/AR
      CFASLP=CAED
      CFB=C.C
C                         CFT IS RAT DRAG
      CFT=C.CC32
      PESI=2.14678-1.1143S*M+.22989*M*M
      FE=PESI*F
      AINFB=A1*BLDCB
      AE=9.3*.0006451G
      TRN1=P*AINFB*1.4*M*N
      TRN2=P*AE
      WDCT=(CFT*AINFB*PMDPT)/SQTINF
      XMCE=WDCT*SGRT(TT-222.)/(PE*AE)
      XME=FRCN(1.4,XMCE)
      TRN3=PE*AE*(1.+1.4*XME*XME)
      CFC=-((TRN1+TRN2-TRN3)/(G*AR))
      RETURN
100   FORMAT (T6,'ALVRJ INLET CATA DEC 1975 ,TOL=',F7.6)
C
C     END
C
CCC
C
      FUNCTICN INTRP (AH,AL,BH,BL,FH,FM)
C
      REAL INTRF
      C2 = AL + (AH - AL)*FN
      C1 = BL + (BH - BL)*FH
      INTRF = C1 + (C2 - C1)*FH
      RETURN
      END
C
CCC
      FUNCTICN FATAS(GAM,XN)
CFATAS      FUNCTICN SUBPRCGRAM TO CALCULATE A CVER ASTAR
C           FRCM GAMMA ANC MACH NUMBER
C
      Z=(GAM+1.C)/(2.0*(GAM-1.C))
      A=2.C/(GAM+1.0)
      B=(GAM-1.0)/2.0
      C=1.C/XN
```

```fortran
      C=A*(1.C+(E*XN*XM))                                          FATA008C
      FATAS=C*(C**Z)                                               FATA009C
      RETURN                                                       FATA010C
      END                                                          FATA011C

C                                                                  R  2
C                                                                  R  4
      FUNCTION FIXAC (A)                                           R  6
C                                                                  R  8
   10 TFIX=AES(A)-1.0000005                                        R 10
      IF(TFIX.LT.0.0) GO TC 1C                                     R 12
      IF(A.LT.0.0) GO TO 20                                        R 14
      FIXAC=C.C                                                    R 16
      GO TO C                                                      R 18
   20 FIXAC=3.1415265                                              R 20-
   30 CONTINUE
      RETURN
      END

C                                                                  S  2
C                                                                  S  4
      FUNCTION FIXAS (A)                                           S  6
C                                                                  S  8
   10 TFIX=AES(A)-1.0000005                                        S 10
      IF(TFIX.LT.0.0) GC TC 20                                     S 12
      IF(A.LT.0.0) GO TO 20                                        S 14
      FIXAS=1.57079633                                             S 16
      GO TO C                                                      S 18
   20 FIXAS=-1.57079633                                            S 20-
   30 CONTINUE
      RETURN
      END

C                                                                  FMAR003C
C                                                                  FMAR001C
CFMARH                                                             FMAR002C
      FUNCTION FMARH (GAM,ATAS)                                    FMAR004C
C     FUNCTION SUBPROGRAM TO CALCULATE MACH NUMBER                 FMAR005C
C     FRCM ATAS AND GAMMA                                          FMAR006C
C                                                                  FMAR007C
      Z = (GAM + 1.0) / (2.C*(GAM - 1.0))                          FMAR008C
      CXMG = 10.0                                                  FMAR009C
      XMG = 10.C                                                   FMAR010C
  5CC CXMG = CXMG / 2.0                                            FMAR011C
      XMG= AMAX1(1.0,AMIN1(100.0,XMG))
      IF(CXMG - 1.CCOC015)1CC,1C0,200
  200 CATAS = 1.0/XMG*(2.0+ (GAM - 1.0) *XMG **2 )/(GAM + 1.0))**Z
      IF(CATAS - ATAS)700,100,800
```

```
700   XMG = XMG + DXMG
      GO TO 50
800   XMG = XMG - DXMG
      GO TO 50
100   FMARL = XMG
      RETURN
      END

      FUNCTION FMARL(GAM,AR)

C     FUNCTION ROUTINE TO FIND MACH FROM A/A* AND GAMMA
C     USING NEWTONS METHOD FOR FINDING ROOTS OF AN EQUATION

C     SUBSONIC SOLUTION
      IF(GAM.LT.1.) WRITE(6,30)
      IF(GAM.LT.1. .OR. AR.LT.1.) CALL EXIT
      GM1=GAM-1.
      GP1=GAM+1.
      A=2./GP1
      B=GM1/(2.*GP1)
      Z=GP1/(2.*GM1)
      IF(AR.LT.1.3401) XMP=2.4706-(1.47059*AR)
      IF(AR.GT.1.34 .AND. AR.LT.3.001) XMP=.77443-(.2048*AR)
      IF(AR.GT.3.) XMP=(A**Z)/AR
      TOL=.0001
10    CONTINUE
      BRACK=A+(B*XMP*XMP)
      POWER=BRACK**Z
      TOP=(1./XMP)-(AR/POWER)
      BOTTOM=(1./BRACK)-(1./(XMP*XMP))
      XM=XMP-(TOP/BOTTOM)
      DELTA=ABS(XM-XMP)
      XMP=XM
      IF(DELTA.GT.TOL) GO TO 10

      FMARL=XM

      RETURN

30    FORMAT('GAMMA LT 1 IN FMARL')
40    FORMAT('A/A* LT 1 IN FMARL')

      END
```

FMAR0120
FMAR0130
FMAR0140
FMAR0160
FMAR0170
FMAR0180

```
C     FUNCTION FMPHIM (GAM , PHI )                                    FMPHO020
C                                                                     FMPHO01C
CFMPHIM   FUNCTION SUBPROGRAM TO CALC MACH NO  FROM PHIM              FMPHO03C
C                                                                     FMPHO040
      TOL = .00001                                                    FMPHO05C
      XMSN = 1.0 / ( PHI**2 )                                         FMPHO060
  127 X = XMSN                                                        FMPHO070
      XMSN = (1.0 +(GAM*(XMSN**2))) / (PHI * SQRT(2.0 * (GAM+1.0)*(1.0 FMPHO090
     1+(GAM-1.0)*.5*(XMSN**2))))                                      FMPHO10C
      XMSN = AMAX1(0., AMIN1(1.0,XMSN))                               FMPHO11C
      IF(ABS(X-XMSN)-TOL) 125, 125, 128                              FMPHO12C
  128 XMSN = (X + XMSN) / 2.0                                         FMPHO13C
      GO TO 127                                                       FMPHO140
  125 FMPHIM = XMSN
      RETURN
      END
CCC
      FUNCTION FMPOPT (GAM,POPT)                                      FMPO0030
CCC
CFMPOPT   FUNCTION SUBPROGRAM TO CALC  XMACH                          FMPO0010
C              FROM P/PT AND GAMMA                                    FMPO0020
C
      Z = (FCPT) ** ((1.0- GAM)/ GAM)                                 FMPO0040
      SMPPT = ( Z - 1.0)/(GAM - 1.0) * 2.0                            FMPO0050
      FMPOPT = SQRT(SMPPT)                                            FMPO0060
      RETURN                                                          FMPO0070
      END                                                             FMPO0080
CCC
      FUNCTION FHIM (GAM, XMCH)                                       FHI002C
CCC
CHIM   FUNCTION TO CALC PHI FROM GAMMA AND MACH                       FHI0010
C
      PHIM = (1.0+GAM *(XMCH **2))/(XMCH * SQRT(2.0*(GAM + 1.0)*(1.0+  FHI003C
     1.5 *(GAM -1.0) * (XMCH **2))))                                  FHI004C
      RETURN                                                          FHI005C
      END                                                             FHI0060
CCC
      FUNCTION FPOPT (GAM,XMACH)                                      FP00030
CCC
CFPCPT   FUNCTION SUBPROGRAM TO CALC TOTAL PRESSURE RATIO             FP00010
C              FROM GAMMA AND MACH NO.                                FP00020
```

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```
C
      Z = -GAM /(GAM - 1.0)
      FPOPT =    (1.0+.5*(GAM -1.0)*(XMACH**2))**Z                      FP00040
      RETURN                                                            FP00050
      END                                                              FP00060
                                                                       FP00070
C
CCC   FUNCTION FRCM(GAM,XMCIR)
C
CCC   FUNCTION ROUTINE TO COMPUTE MACH NUMBER FROM
CCC   MCIRCLE AND GAMMA FOR ALL MACH NUMBERS USING NEWTONS METHOD
C
      IF (GAM.LT.1.) WRITE (6,100)
      IF (GAM.LT.1.) CALL EXIT
      A=GAM
      B=0.5*(GAM-1.)
      C=XMCIR/.5902063
      XMP=C/(1.18+(.0923*C))
      TOL=.0001
   10 CONTINUE
      BRACK=A+(B*XMP*XMP)
      POWER=SQRT(BRACK)
      TOP=(XMP*POWER)-C
      BOTTOM=(A+(2.*B*XMP*XMP))/POWER
      XM=XMP-(TOP/BOTTOM)
      DELTA=ABS(XM-XMP)
      XMP=XM
C
      IF(DELTA.GT.TOL) GO TO 10
C
      FRCM=XM
C
      RETURN
C
  100 FORMAT('GAMMA LT 1 IN FROM')
      END
C
CCC   FUNCTION FTOTT (GAM,XMACH)
C
CCC   FUNCTION SUBPROGRAM TO CALC T/TT    FROM    GAMMA AND MACH NO      FT00020
C                                                                      FT00010
      FTOTT    =   (1.0+.5*( GAM-1.0)*(XMACH**2))**(-1.0)              FT00030
      RETURN                                                           FT00040
      END                                                             FT00050
C
```

```
C
C     SUBROUTINE TAB(FAS)
C
      WRITE(6,15)
15    FORMAT (16,'NO.2 JP5 AND JETA FUEL MAY 1,1976 ONE ATM     ')
      FAS= 14.6394
      RETURN
      END
C
CCC
C     FUNCTION FMCIR (GAM,XM)
C
C     MCIRCLE  FUNCTION SUBPROGRAM TO CALC MCIR FROM GAMMA AND MACH NO
C     R AIR= 8314.34/28.9624E = 287.073 N*M/KG*K
C     M CIRCLE DIMENSIONS = SEC * SQRT(K) / METRE
C
      FMCIR=.C59C2C6289*XM*SQRT(GAM*(1.0+((GAM-1.0)/2.0)*XM**2))
      RETURN
      END
C
CCC
      SUBROUTINE AIR (Z,V,J,P,T,S,D,Q,GO,K,KK)
C
C     Z=ALTITUDE IN METERS
C     V=MACH NUMBER OR VELOCITY, SEE KK
C     J=FIRST PASS IDENTIFIER SWITCH, -=FIRST PASS AND +=NOT FIRST PASS
C     P=PRESSURE IN PASCALS OR PSI
C     T=TEMPERATURE IN K OR R
C     S=SPEED OF SOUND IN METERS/SEC OR FT/SEC
C     D=DENSITY IN KG/CUBIC METER OR LBM/CUBIC FOOT
C     G=DYNAMIC PRESSURE IN PA OR PSI
C     GO=LOCAL GRAVITY IN FT/SEC2 OR METERS/SEC2
C     K=1, SI UNITS
C     K=2, ENGLISH UNITS
C     KK=1, V IS MACH NUMBER
C     KK=2, V IS VELOCITY, METERS/SEC OR FT/SEC
C
      DIMENSION A(2,16), C(15)
C
C***  THESE ARE THE CHEBYSHEV COEFFICIENTS FOR P/F0
C         A(1,J),J=1,16
C***  THESE ARE THE CHEBYSHEV COEFFICIENTS FOR D/DO
C         A(2,J),J=1,16
```

```
      DATA A/
     A-4.0135170, -4.0135170, -2.2874890, -2.1765372,
     B-1.0494210, -.1358554, -.0355105, -.0498002,
     C -.0002626, -.0006161, -.0030910, -.0121008,
     D -.0001016, -.0002977, -.0004221, -.0044266,
     E -.0000145, -.0003573, -.0000523, -.0001313,
     F -.0000031, -.0021286, -.0002918, -.0001147,
     G-1.0001420, -.0010109, -.99998983, 1.0000000/
C **  SET CONSTANTS
C
      DATA PC,EC,RBAR,GC,Z1/
     1101325.0,1.225,287.07299,9.80665,30480.0/
C **  IF NECESSARY , CONVERT TO SI UNITS
C       Z BECOMES METERS
C       V BECOMES METERS/SEC
C
      IF (K.EQ.2) Z=Z*.3048
      IF (K.EQ.2.AND.KK.EQ.2) V=V*.3048
C **  START HERE
C
      IF (J) 10,20,20
   10 WRITE (6,60) Z1
      WRITE (6,70) Z1
C **  COMPUTE C(K) COEFFICIENTS
C
   20 ETA=2.*Z/Z1-1.
      C(1)=ETA
      C(2)=ETA**2-2.
      DO 30 I=3,15
   30 C(I)=ETA*C(I-1)-C(I-2)
C **  COMPUTE CHEBYSHEV TRUNCATED EXPANSION
C
      ALNP=A(1,1)
      ALND=A(2,1)
      DO 40 I=2,15
      ALNP=ALNP+A(1,I)*C(I-1)
   40 ALND=ALND+A(2,I)*C(I-1)
C **  COMPUTE ATMOSPHERIC PRESSURE
C       P IN N/SQ METER
C
      ALNP=.5*ALNP
```

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```
      FOFZ=EXF(ALNP)
      F = FCF2*FC*A(1,16)
C
C **   COMPUTE GRAVITY AT ALTITUDE AND LATITUDE
C          RE IS EQUATORIAL RADIUS (M) PER CRC HANDBOOK
C          GC IN M/SEC SQ
      RC=6378377.45
      GC=GC*((RC/(RO+Z))**2)
C
C **   COMPUTE ATMOSPHERIC DENSITY
C          D IN KG PER CUBIC METRE
      ALND=.5*ALND
      DODZ=EXF(ALND)
      D = DCDZ*CC*A(2,16)
C
C **   COMPUTE AIR TEMPERATURE
C          T IN DEGREE KELVIN
      T=P/(REAR*D)
C
C **   COMPUTE SPEED OF SOUND IN M/SEC
      S=SQRT(401.90219*T)
C
C **   COMPUTE DYNAMIC PRESSURE IN PA
      IF (KK.EG.1) Q=0.7*F*V**2
      IF (KK.EG.2) Q=0.7*P*(V/S)**2
C
C **   CONVERT TO ENGLISH UNITS IF NECESSARY
      IF (K.EG.1) CC TO 50
      Z=Z/.3048
      IF(KK.EG.2) V=V/.3048
      P=P/6894.757
      T=T*1.8
      S=S/.3048
      D=D/16.C1846
      Q=Q/689.4.757
      GC=GC/.3048
      RETURN
   50 FORMAT (T9,'*** US 1962 STANDARD ATMOSPHERE')
   70 FORMAT (T9,'*** ALTITUDE FROM 0 TO ',F8.0,' METERS')
      END
```

```
      FUNCTION ANORM(A,B)
C
C     CALCULATES TOTAL PRESSURE RATIO ACROSS A NORMAL SHOCK
C     A=GAMMA,B=XMACH
C
      C=(A+1.)/2.
      CC=(A-1.)/2.
      EE=(2.*A)/(A+1.)
      F=(A-1.)/(A+1.)
      G=A/(A-1.)
      H=1./(A-1.)
      BB=B*B
      ANUM=((C*BB)/(1.+CC*BB))**G
      DEM=((EE*BB-F)**H)
      ANORM = ANUM/DEM
      RETURN
      END

      FUNCTION FPMCPT( GAM ,XM )
C
C     FUNCTION SUBPROGRAM TO CALCULATE P/PT * M CIRCLE
C     FROM GAMMA AND MACH NUMBER
C     DIMENSIONS = SEC * SQRT(K) / METRE
C
      FPMCPT = FMCIR ( GAM , XM ) * FPOPT ( GAM , XM )
      RETURN
      END

      SUBROUTINE SERCH (X,A,J,I,M)
C
      DIMENSION A(20)
      DO 10 L=1,I
      J=L
      IF (X.LE.A(L)) GO TO 20
   10 CONTINUE
   20 IF (J.EG.1) GO TO 30
      J=J-1
   30 RETURN
      END

C
      FUNCTION SHOCK(XM,C)
```

```
C     SHOCK FUNCTION SUBPROGRAM TO CALCULATE THE OBLIQUE SHOCK ANGLE FROM
C     THE WEDGE ANGLE AND MACH NUMBER
C     XM=MACH NUMBER C=WEDGE ANGLE DELTA IN RADIANS
C     SHOCK=SHOCK ANGLE THETA IN RADIANS
C     P,Q,R,A,B=CONSTANTS F=PHI WHICH IS AN INTERMEDIATE ANGLE
C     RADEG=TRANSFORMS RADIANS TO DEGREES

      RADEG = 57.29577951301
      SINZDZ = SIN(C)
      P=-((XM*XM+2.)/(XM*XM)) -(1.4*SINZDZ*SINZDZ)
      CQ=1.44+((4./(XM*XM))
      Q=((2.*XM*XM)+1.)/(XM*XM*XM*XM)+(CQ*SINZDZ*SINZDZ)
      R=(-C*C)/(XM*XM*XM*XM)
      A=(1.-/3.)*(3.*Q-P*P)
      B=(1./27.)*(2.*P*P*P-S.*P*Q +27.*R)
      TEST=(B*B)/4.+((A*A*A)/27.)
      IF(TEST)1,1,2
    1 CONTINUE
      F=ARCCS((-B/2.)/SQRT((-1./27.)*A*A*A))
      FO=F*RADEG
      FOX=(FO/3.)+240.
      FOXE=(FOX)/RADEG
      X=2.*SQRT(-A/3.)*COS(FOXE)
      SHOCK = ARSIN(SQRT(X-P/3.))
      RETURN
    2 WRITE(6,3)
    3 FORMAT(48H THW CONE THE INPUTS TO SHOCK GIVE COMPLEX ROOTS)
      RETURN
      END
```

```
      FUNCTION STDLI (TBX,TBY,TAB,X,Y,NX,NY)
C     FUNCTION DESIGNED TO ALLOW THE USER TC INPUT
C     VARIABLE LENGTH TABLES. IT INTERPOLATES FIRST IN THE X
C     VARIABLE AND THEN IN THE Y VARIABLE. IT EXTRAPOLATES FROM
C     THE FIRST OR LAST INTERVAL IF THE X CR Y IS OUTSIDE OF THE
C     BOUNDS OF THE TABLE. IT REQUIRES THE SUBROUTINE SERCH FOR
C     ITS OPERATION.
C
C     PROGRAMMER -- H.SOBEL      30 OCTOBER 1967

      DIMENSION TBX(NX), TBY(NY), TAB(11,11)
      CALL SERCH (X,TBX,I,NX,1)
      CALL SERCH (Y,TBY,J,NY,1)
      XX=TBX(I)
```

```
      YY=TEY(J)
      TXY=TAB(I,J)+(X-TBX(I))*((TAB(I+1,J)-TAB(I,J))/(TBX(I+1)-TBX(I)))
      XJ=TAB(I,J+1)+(X-TBX(I))*((TAB(I+1,J+1)-TAB(I,J+1))/(TBX(I+1)-TBX(I)))
      XJ1=TAE(I,J+1)+(X-TBX(I))*((TAB(I+1,J+1)-TAE(I,J+1))/(TBX(I+1)-TBX(I))-TEX
     1(I))))
      STDL=XJ+(Y-TEY(J))*((XJ1-XJ)/(TBY(J+1)-TEY(J)))
      STCLI=STCL
 1C   RETURN
      END
```

```
      FUNCTICN STCLIA (TBX,TBY,TAB,X,Y,NX,NY)
C
C        FUNCTICN CESIGNED TO ALLCW THE USER TO INPUT
C     VARIAELE LENGTH TABLES.  IT INTERPOLATES FIRST IN THE X
C     VARIAELE AND THEN IN THE Y VARIABLE.  IT EXTRAPOLATES FROM
C     THE FIRST OR LAST INTERVAL IF THE X CR Y IS OUTSIDE CF THE
C     BOUNCS CF THE TAELE.  IT REQUIRES THE SLBROUTINE SERCH FOR
C     ITS CPERATION.
C
C        FFCGRAMMER -- H.SOBEL      30 OCTOBER 1967
C
      CIMENSION TBX(NX), TBY(NY), TAB(NX,NY)
      CALL SERCH (X,TBX,I,NX,IC)
      CALL SERCH (Y,TBY,J,NY,JC)
      XJ=TAB(I,J)+(X-TBX(I))*((TAB(I+1,J)-TAB(I,J))/(TBX(I+1)-TBX(I)))
      XJ1=TAE(I,J+1)+(X-TEX(I))*((TAB(I+1,J+1)-TAE(I,J+1))/(TEX(I+1)-TEX
     1(I)))
      STCLI=X J+(Y-TEY(J))*((XJ1-XJ)/(TBY(J+1)-TBY(J)))
      STDLIA=STCLI
 10   RETURN
      END
```

```
      SUBRCUTINE SUBSON(H,ZM,F,C,W,Q,A)
C
C
      C=.3
      SFC=3.C
      THR=.2248C5*C*Q*A
      WF=(SFC*THR)/3690.
      W=WF*.45556
      IF(W.LT. 0.0)W=-W
      RETURN
      END
```

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```
C     FUNCTION VECMAG(X)
C
      FUNCTION VECMAG(X)
      DIMENSION X(3)
   10 X2=X(1)*X(1)+X(2)*X(2)+X(3)*X(3)
      VECMAG=SQRT(X2)
      RETURN
      END

      FUNCTION TC (T,ER,ATM)
C
C     THEORETICAL TEMPERATURE RISE CORRECTION FOR PRESSURES OTHER
C     THAN ONE ATMOSPHERE (HYDROCARBON FUELS)
C
      DIMENSION C(8),E(31),G(31,3),P(13),H(13,2)
      DATA  /-.1254034E4,-.19116E3,.74669SE2,-.397487E2,-.26
     170 1E2,-.13558305E2,-.108508092E2/
      DATA E /-.55,-.05,-1.05,-1.55,-2.25,-35.,-45.,-55.,-6.,-65.,-7.,-75.,-8.
     1-.85,-.95,-1.05,-1.15,-1.25,-1.35,-1.45,-1.45,-1.5,-1.5,-1.5,-1.5,-1.75,-.8
      DATA G /.0005248,-.000552,-.000084,.000258,-.001837,-.00407,-.007
     1903626,-.014747,-.025548,-.03164,-.065907,-.097195,-.13662,-.18292,-.2
     236262,-.29312,-.36713,-.40644,-.453286,-.225566,-.188211,-.157010,-.459541,-.00
     3-.418C49,-.00414,-.0004545,-.013411,-.003851,-.0825,-.082221,-.0078566,-.263936,-.22
     4-.0,-.00144,-.019840,-.198405,-.532892,-.29157,-.29268,-.429214,-.032921,-.0
     557-.2107C,-.053804,-.0148795,-.019739,-.53289,-.36897,-.341905,-.225221,-.00244,-.2
     6-.1771C,-.035121,-.0085128,-.019739,-.03957,-.071765,-.114441,-.173804,-.22253,-.0
     7-.0C1710,-.01242,-.0008436,-.020717,-.03895,-.0844450,-.21432,-.205284,-.08215,-.1
     8-.0C144,-.005804,-.0004545,-.0032,-.048546,-.08488,-.47144,-.2643349,-.00121,-.1
      DATA P /-.341366,-.25190/
      DATA H /-.20,-.35,-.50,-.75,-1.00,-.75,-5,-3.5,-5.,-7.,-10.,-15.,-20./.298846
     1-.36326,-.44161,-.297035,-.1809,-.066615,-.1027180,-.1661,-.77316,-.2282
     27-.C4842E.0,-.075181,.08051,-.574833,-.60759,-.80970,-.02264,-.121555,-.21910,-.37
     3.927,-.4E712/
C
C     CHECK FOR ENTRY OUTSIDE LATTICE
C
      IF (T.LT.258.) GO TO 50
      IF (T.GT.1300.) GO TO 60
      IF (ER.GT.1.5) GO TO 70
      IF (ATM.LT.2) GO TO 90
      IF (ATM.GT.20.) GO TO 80
C
C     COMPUTE FACTOR ANALYSIS FACTORS F1,F2,F3
C
```

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```
      F1=-((.227276E-3+.100807E-6*T)*T+.018785)
      F2=((.0012009E-.1254E-5*T)*T+.0846043
      F3=(((.113312E-7-.24417E-11*T)*T-.141615E-4)*T+.0049629S)*T+.0056
      A0473
C
C     LINEARLY INTERPOLATE FOR FACTORS G1,G2,G3
C
      DO 10 I=1,31
      IF(ER.LE.E(I)) GO TO 20
   10 CONTINUE
   20 J=I-1
      R=(ER-E(J))/(E(I)-E(J))
      G1=G(J,1)+((G(I,1)-G(J,1))*R
      G2=G(J,2)+((G(I,2)-G(J,2))*R
      G3=G(J,3)+((G(I,3)-G(J,3))*R
C
C     LINEARLY INTERPOLATE FOR FACTORS H1,H2
C
      DO 30 I=1,13
      IF(ATM.LE.P(I)) GO TO 40
   30 CONTINUE
   40 J=I-1
      R=(ATM-F(J))/(P(I)-P(J))
      H1=H(J,1)+(H(I,1)-H(J,1))*R
      H2=H(J,2)+(H(I,2)-H(J,2))*R
C
C     COMPUTE TEMPERATURE CORRECTION (TC)
C
      TC=C(1)*F1*G1*H1+C(2)*F2*G2*H1+C(3)*F1*G2*H1+C(4)*F2*G1*H2
     +   +C(5)*F3*G3*H1
     +   +C(6)*F2*G3*H2
     +   +C(7)*F3*G2*H2
     +   +C(8)*F1*G3*H2
C
   50 RETURN
   60 WRITE(6,110)
      GO TO 100
   60 WRITE(6,120)
      GO TO 1CC
   70 WRITE(6,130)
      GO TO 1CC
   80 WRITE(6,150)
      GO TO 1CC
   SC WRITE(6,140)
  100 CALL EXIT
      RETURN
C
```

```
110   FORMAT (' O TOTAL TEMPERATURE LESS THAN 298 K. END RUN.')
120   FORMAT (' O TOTAL TEMPERATURE GREATER THAN 1300 K. END RUN.')
130   FORMAT (' O FUEL EQUIVALENCE RATIO EXCEEDS 1.5 END OF RUN.')
140   FORMAT (' O ATMOSPHERIC PRESSURE LESS THAN 0.2, END OF RUN.')
150   FORMAT (' O ATMOSPHERIC PRESSURE EXCEEDS 20, END OF RUN.')
      END

C
C

      FUNCTION CDLI (A,X,F,N)
      DIMENSION X(N),F(N)
      IF (A-X(1)) 50,10,10
10    IF ((X(N)).EQ.X(2).OR.X(N-1).EQ.X(N)) GO TO 70
      CALL SERCL(X(2),I,A,C)
      IF (4*A-X(I+1)-X(I+2)) 20,40,20
20    CDLI=F(I)
      RETURN
30    CDLI=F(I)+(A-X(I))*(F(I+1)-F(I))/(X(I+1)-X(I))
      RETURN
40    CDLI=0.5*(F(I+1)+F(I+2))
      RETURN
50    WRITE (6,90)
      GO TO 100
60    WRITE (6,100)
      GO TO 110
70    WRITE (6,110)
80    CALL EXIT
90    FORMAT(1H1,10X,57HERROR IN SUBROUTINE ODLI, TABLE HAS LESS THAN T
     1HREE ENTRIES)
100   FORMAT(1H1,10X,60HERROR IN SUBROUTINE ODLI, INITIAL AND FINAL FCI
     1UALS ARE EQUAL)
110   FORMAT (1H1,10X,59HERROR IN SUBROUTINE CDLI, DISCONTINUITY AT ONE
     1END OF TABLE)
      END

C
C

      SUBROUTINE INTR20(X1,X2,C,D,L)
      DIMENSION C(1900)
      X=X1
      Y=X2
      N1=C(1)
      N2=C(2)
      IX1=N1+2
```

```
      DO 10 II=4,IX1
      I=II
      IF(X.LT.C(II)) GO TO 11
10    CONTINUE
11    IO=I-4
      IX2=IX1+4
      IX3=IX1+42
      DO 20 JJ=IX2,IX3
      J=JJ
      IF(Y.LT.C(J)) GO TO 21
20    CONTINUE
21    JO=J-IX1
      NA=IX3+42*((L-1)*N1+IC-2)+JO-1
      F1=((X-C(I-1))/(C(I)-C(I-1)))
      F2=((Y-C(J-1))/(C(J)-C(J-1)))
      F3=F1*F2
      C= C((NA)*(1.-F1-F2+F3)
     1 + C((NA+1)*(F1-F3)
     2 + C((NA+1)*(F2-F3)
     3 + C((NA+1)*F3
      RETURN
      END


      FUNCTION THREDL (X,Y,Z,AX,AY,AZ,AXYZ,NX,NY,NZ)                  F 2
C     THIS FUNCTION INTERPOLATES LINEARLY IN THREE DIMENSIONS. IT     F 4
C     SELECTS THE TWO PLANES OF CONSTANT Z AND USES STDLI FOR TWO     F 6
C     DIMEN-                                                          F 8
C     SIONAL INTERPOLATION. A LINEAR INTERPOLATION IS USED IN Z.      F 10
C     PROGRAMMER H.SOBEL          DATE 22 AUGUST 1968                 F 12
      DIMENSION AX(NX), AY(NY), AZ(NZ), AXYZ(NX,NY,NZ)                F 14
      DATA .../SEFECT. (Z,AZ,K,NZ,M)                                  F 16
      CALL SEFECT (Z,AZ,K,NZ,M)                                       F 18
      AL=STDLIA(AX,AY,AXYZ(1,1,K),X,Y,NX,NY)                          F 20
      AU=STDLIA(AX,AY,AXYZ(1,1,K+1),X,Y,NX,NY)                        F 22
      THREDL=AL+(AU-AL)*(Z-AZ(K))/(AZ(K+1)-AZ(K))                     F 24
      RETURN                                                          F 26-
      END
```

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